Aberfeldy New Village Masterplan Environmental Statement Volume 3: Technical Appendices

Appendix: Water Resources, Drainage and Flood Risk

Annex 1: Flood Risk Assessment

Annex 2: Drainage Strategy

Annex 3: Thames Water – Potable Water Supply Correspondence Annex 4: Sustainable Urban Drainage System (SuDS) Proforma

Aberfeldy Village, London

Masterplan, Below Ground Drainage Strategy
Stage 2+ Planning Issue

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Aberfeldy Village, London Masterplan, Below Ground Drainage Strategy



ABERFELDY VILLAGE, LONDON BELOW GROUND DRAINAGE STRATEGY ISSUED FOR PLANNING

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Aberfeldy Village, London Masterplan, Below Ground Drainage Strategy



Executive Summary

Meinhardt UK Ltd has been appointed by Ecoworld International to undertake the foul and surface water below ground drainage design for the proposed construction of Aberfeldy Village. The scheme consists of approximately 1500 units proposed across multiple Phases. The proposals comprise of a number of blocks including podiums and some towers up to 29 stories in height. The Site is located within the London Borough of Tower Hamlets in an area known as Poplar Riverside, Aberfeldy Village, E14, London.

The proposed surface water drainage strategy for each phase has been developed to utilise sustainable drainage techniques (SuDS) to attenuate surface water at source and reduce the risk of downstream flooding of the Thames Water sewer network in the local area. A scheme has been developed that utilises blue, green and podium deck attenuation roof structures along with below ground cellular attenuation tanks designed for the 1:100 year plus 40% climate change storm event.

The developments QBAR greenfield runoff rate has been calculated to be 18.8l/s. It is proposed that the entire site will discharge at this rate as agreed with the London Borough of Tower Hamlets. Each building and associated hardstanding being proposed to discharge at a proportion of this flow rate, this has been split between 12 separate connections across the site receiving the total 18.8l/s. Each buildings associated storm water drainage is conveyed by a traditional gravity run system to the nearest Thames Water Asset, with all connection discharging into the Thames Water combined water Sewer network.

The proposed foul water drainage strategy for the site involves the MEP engineer's coordination of the superstructure drainage up until it exits the buildings and enters the below ground drainage network. A below ground drainage network of pipes and manholes will collect the foul water discharge from the buildings and convey to a demarcation chamber, before discharging via gravity to the existing Thames Water combined water sewers within the site or surrounding the site. This will be coordinated during detailed design.

A pre planning enquiry has been submitted to Thames Water stating the proposed foul and surface water discharge rates from the new development. Thames water had responded giving approval for both however, new plans have been submitted since and flow rate applied from the scheme has reduced from that agreed in the pre planning, it is therefore assumed this is still accepted.

The Thames Water asset records for the site highlighted potential foul and surface water connection points however further CCTV survey works will need to be undergone before any detailed design.

Refer to drainage drawings 2812-MHT-CV-BG-DR-100 and 2812-MHT-CV-RF-DR-101 within the appendix for proposed drainage layout.



1 Introduction

This Drainage Strategy Report has been prepared by a Meinhardt and is submitted in support of a hybrid planning application for the Aberfeldy Village Masterplan. The hybrid planning application is made in relation to the north of East India Dock Road (A13), east of the Blackwall Tunnel Northern Approach Road (A12) and to the southwest of Abbot Road (the "Site") on behalf of The Aberfeldy New Village LLP' ("The Applicant"). The hybrid planning application is formed of detailed development proposals in respect of Phase A for which no matters are reserved ("Detailed Proposals"), and outline development proposals for the remainder of the Site, with all matters reserved ("Outline Proposals"). The Detailed Proposals and Outline Proposals together are referred to as the "Proposed Development".

The Proposed Development comprises the comprehensive redevelopment of the Site. The Proposed Development will provide new retail and workspace floorspace along with residential dwellings and the pedestrianisation of the A12 Abbott Road vehicular underpass to create a new east to west route. The Development will also provide significant, high quality public realm, including a new Town Square, a new High Street and a public park.

The purpose of the Drainage Strategy Report is to assist our client and the Local Planning Authority to make an informed decision regarding the drainage strategy for the proposed development in addition to assist the BREEAM assessor with the rewarding of credits under Pol 03.

Aberfeldy Village, London Masterplan, Below Ground Drainage Strategy



2 Existing Drainage

1.1 Existing Site

The existing site is located in an area known as Poplar Riverside, Aberfeldy Village, E14, London, within the London Borough of Tower Hamlets.

The existing site is a mixed-use development consisting of residential housing and non-residential floor space, including shops, professional services, food and drink, residential institution, storage, community and cultural uses.

The Site is located in Poplar, within the administrative boundary of the London Borough of Tower

Hamlets. The Site is 8.14 hectares (approx. 20 acres) in total and comprises:

- Abbott Road;
- Aberfeldy Street;
- Balmore Close;
- Blairgowrie Court;
- Heather House;
- Jura House;
- Tartan House;
- Thistle House;
- Kilbrennan House;
- Nos. 33-35 Findhorn Street;
- 2a Ettrick Street;
- 384 Abbott Road;
- Lochnagar Street;
- Aberfeldy Neighbourhood Centre;
- Nairn Street Estate; and
- Leven Road Open Space and Braithwaite Park are included for their enhancement.'

The site area totals Circa 4.92ha, excluding council adopted roads and green areas the total hardstanding is 3.0ha.

The River Lee is located to the east of the site and flows in a generally southerly direction to its confluence with the River Thames. The entire site is noted on the Gov.uk website's Flood map for planning to be wholly within flood zone 3 however benefits from the presence of flood defences.



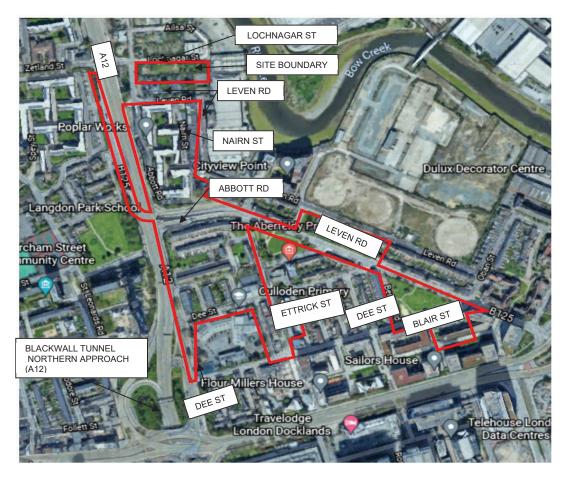


Figure 1: Site Location

Aberfeldy Village, London Masterplan, Below Ground Drainage Strategy



1.2 Existing Drainage

1.2.1 Private Onsite Drainage

A topographical survey of the site has been completed by Aworth Survey in December 2009 and a utility survey was carried out for the site by Sumo Services Survey in August 2020.

Based on these surveys the existing private drainage network consists of surface water, foul water and combined water pipes and manholes. All of the existing private drainage has been shown to be draining to the closest Thames Water public sewer via multiple existing connections to the Thames Water surface and combined water sewers crossing through the site.



Figure 2: Topographical Survey

A CCTV survey will be undertaken to confirm the exact line, level, and condition of the connections to the surrounding public sewer network.

A copy of the topographical and utility surveys can be found in the appendices.



1.2.2 Public Sewers

Asset records obtained in November 2020 from Thames Water have revealed public surface and combined water sewers crossing through the proposed Aberfeldy Village site. The arrangement of the network is summarised below:

Thames Water Surface Water Sewers

The surface water sewers crossing the proposed site are located within:

- Abbott Road (B125) within the proposed site boundary (From MH Ref: 3406 3403 to 3402). The diameter of the surface water sewer is 225mm;
- Abbott Road (B125) within the proposed site boundary (From MH Ref: 2420 3403 to 3402). The diameter of the surface water sewer is 225mm. It is assumed to be a Thames Water pumping station for the road fly under. A CCTV survey will be required to establish what it serves.

These two sewers are assumed to be picking up Abbott Roads highway drainage and will therefore be abandoned along with the road itself as dictated by the scheme.

Thames Water Combined Water Sewers

The combined water sewers crossing the proposed site are located within:

- Lochnagar Street to the north of the site (the public combined water sewer is running west within Lochnagar Street to MH Ref: 2704). The diameter of the combined water sewer is 305mm and changes to 381mm just before connecting into Thames Water manhole 2704;
- Bromley Hall Road to the north west of the site (From MH Ref: 2630 to 2705). The diameter of the combined water sewer is 225mm and changes to 305mm just before connects to Thames Water manhole 2705:
- Leven Road to the east of the site (the public combined water sewer is running south within Leven Road: from MH Ref: 3605 to 5403). The diameter of the combined water sewer starts at 225mm and increases in size to 300mm sewer. The combined water sewer then changes into a 600mm before entering the proposed site and connecting into Thames Water combined manhole 5403;
- Leven Road to the east of the site (the public combined water sewer is running north within Leven Road: from MH Ref: 7403 to 5405). The diameter of the combined water sewer starts at 305mm, changes in size to 300mm sewer and then to 225 before connecting into Thames Water combined manhole 5405;
- Darnaway Place to the east of the site (the public combined water sewer is running south within Darnaway Place: from MH Ref: 4511 to 4407). The diameter of the combined water sewer is 229mm;
- Blair Street to the south of the site and running north through the proposed site boundary (From MH Ref: 7303 to 6302). The diameter of the combined water sewer is 305mm and changes to 457mm after the junction with Thames Water combined sewer which is running north to the combined Thames Water manhole 6302;
- Blair Street to the south of the site (the public combined water sewer is running east within Blair Street from: MH Ref: unknown-4203 to 5205). The diameter of the combined water sewer is 305mm and changes to 457 before connecting into Thames Water combined manhole 5205;
- Aberfeldy Street within the proposed site boundary (the public combined water sewer entering through the south of the site and is running north within Aberfeldy Street: from MH Ref: 5205 to 4407). The diameter of the combined water sewer starts at 457mm and changes to 533mm before connecting into Thames Water combined water manhole 4301A. The combined water sewer exiting Thames Water manhole 4301A is 610mm and changes to 686mm after Thames Water combined manhole 4420, before connecting into Thames Water combined manhole 4407;

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- Dee Street within the proposed site boundary (the public combined water sewer is running east within Dee Street from MH Ref: 3222 to 4312). The diameter of the combined water sewer is 305mm;
- Ettrick Street within the proposed site boundary (the public combined water sewer is running east from MH Ref: 3316 to 4301A). The diameter of the combined water sewer is 300mm and changes to 305 before connecting into Thames Water combined manhole 4301A;
- Abbott Road (B125) within the proposed site boundary (From MH Ref: 8301 to the combined trunk running north within Joshua Street). The diameter of the combined water sewer is 914mm and changes to 991mm just before connects to the combined trunk in Joshua Street;
- Abbott Road (B125) within the proposed site boundary (From MH Ref: 4407 to the combined trunk running north within Joshua Street). The diameter of the combined water sewer is 991mm.

There is a combined water trunk sewer located to the west of the site within the proposed site boundary running north. The diameter of the combined water sewer is 2250mm.

Refer to the appendices for the complete Thames Water Asset Records.

Meinhardt has overlaid the existing sewer information from the Thames Water Asset Records and the proposed architectural masterplan on a sketch to determine whether there are any areas where proposed structure will sit over the existing Thames Water assets. The sketch has highlighted a number of the proposed buildings are located directly above the existing Thames Water sewers and manholes. Where this occurs either a build over agreement or a sewer diversion will be required with Thames Water to proceed with the current site layout.

Based on the Thames Water Assets Records all of the existing private drainage has been shown to be draining to the north of the site where there are multiple existing connections to the Thames Water surface and combined water sewers crossing through the site.

Refer to the sketch 2812-MHT-CV-BG-DR-050 in the appendices for details of the existing Thames Water sewers crossing the site.



2 Drainage Strategy

2.1 Surface Water Drainage

2.1.1 Drainage Design Parameters

The industry standards along with the Environment Agency and Sewers for Adoption 7th Edition dictate for below ground surface water drainage that:

- There will be no surcharging of the drainage system for a 1 in 2-year storm;
- The drainage can be surcharged with no flooding for a 1 in 30-year storm; and
- The drainage can flood on-site for a 1 in a 100-year storm with a 40% climate change allowance
 provided the flood water remains on site and does not flood habitable areas or affect safe ingress
 and egress to the site for occupiers.

All surface water drainage options outlined in this report adhere to these principles.

Hydraulic calculations have been carried out using the hydraulic modelling software Microdrainage unless otherwise specified.

2.1.2 Initial Consultations

2.1.2.1 Local Authority/Planning Authority – Tower Hamlets Council

Tower Hamlets Council were contacted on 01/09/21 to discuss the proposed drainage strategy prior to planning submissions, however, no response has been received at the time of writing.

2.1.2.2 Thames Water

A predevelopment enquiry has been submitted to Thames Water to confirm if there is sufficient capacity within the Thames Water public sewer network to accommodate the proposed development. Thames Water have confirmed there is sufficient capacity in the surrounding public sewers to accept the flows from the proposed development.

2.1.3 Proposed Surface Water Drainage Strategy

The proposed site will discharge at the equivalent QBAR greenfield rate of 18.8l/s. Hydraulic calculations indicate that the attenuation volume required for the development to discharge at the proposed discharge rate of 18.8l/s for a 1 in 100 year + 40% climate change storm event is approximately 3562m³, to be confirmed during detail design. This strategy should also include measures to improve run-off quality whilst maximising bio-diversity, amenity and other multifunctional benefits to provide a sustainable drainage system as noted in PPG.

Table 2-1: Discharge Opportunities

London Sustainable Drainage Hierarchy	Site Specific Application	
Store rainwater for later use	There are limited opportunities for rainwater harvesting on this project due to the proposed usage of the building and limited external space that requires irrigation. It has therefore been discounted.	

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Use infiltration techniques, such as porous surfaces in non- clay areas	Due to the underlying geology of the site being London Clay and poor infiltration rates, infiltration devices are not used on this site. Furthermore, there are limited locations that comply with the requirement of Building Regulations to be more than 5m from a highway or structure. The use of infiltration techniques has therefore been discounted.
Attenuate rainwater in ponds or open water features for gradual release	Due to the constrained nature of the site, there is little opportunity for above ground storage structures like ponds. Furthermore, the existing levels across the site do not offer any suitable locations where controlled flooding may occur.
Attenuate rainwater by storing in tanks or sealed water features for gradual release	Excess surface water flows during high intensity rainfall events are proposed to be stored using a combination of podium/blue roofs, green roofs bioretention/SuDS planters and below ground geo-cellular storage crates.
Discharge rainwater direct to a water course	Not possible because there are no watercourses in area surrounding site
Discharge rainwater to a surface water sewer/drain	Not possible because there are no surface water drains in area surrounding site, nearby public sewers are combined.
Discharge rainwater to a combined sewer	Discharge to a combined system at the restricted rate equivalent to QBAR greenfield rates.

The proposed surface water strategy for the site will be developed to utilise sustainable drainage techniques (SuDS) to attenuate surface water at source and reduce the risk of downstream flooding. Due to the limited areas of landscaping available on the site there are constraints to which SuDS can be incorporated into the development. SuDS with large land take such as detention basins or ponds are not suitable for an urban development therefore not applicable for development. It is also found that the use of infiltration SuDS will not be feasible for the site due to the existing ground conditions. The proposed drainage strategy for the development has therefore been made sustainable through the use of blue roofs, high level podiums attenuation and below ground attenuation tanks.

It is proposed that each phase will have a separate drainage network.

Phase A Strategy - Detailed Planning Application

Based on the above, the only feasible surface water discharge location is the public sewers surrounding the site. Phase A is divided into 3 different locations therefore it is proposed that Blocks I1, J1, F1, H1&H2 and H3 to drain separately into the closest Thames Water sewer. Therefore the strategy is outlined below.

Block I1:

The proposed surface water drainage strategy for Building I1 has been made sustainable through the use of a blue roof and a below ground attenuation tank. The approximate volume of attenuation for this building is 69m³. Of which 34.2m³ attenuation is provided by cellular attenuation crates and 35m³ is provided by the blue/green roof.



The surface water drainage network will drain via gravity to the northwest of Building I1 into a demarcation chamber restricting the discharge rate to 1l/s which is to be controlled via a hydrobrake, prior to discharging to the Thames Water sewer network. It is proposed that controls will be used on the blue roof to ensure that all attenuation is fully utilised. It is proposed that a new connection will be made to the northwest corner of the building into the Thames Water combined water network in Blair Street (TWMH7303). The Thames Water sewer asset records have no cover level or Invert level information for the manhole THMH7303 therefore a survey is required for the existing combined water sewer running along Blair Street.

Block J1:

The proposed surface water drainage strategy for Building J1 has been made sustainable through the use of a below ground attenuation tank. It is proposed to discharge surface water from Building J1 via gravity into Thames Water combined water sewer in Leven Road (TWMH3602) via a new connection. Surface water discharge from the building is to be restricted to 1.25l/s which is to be controlled via a hydrobrake on a demarcation manhole prior to discharging into Thames Water combined water sewer. The approximate required storage for building J1 is 346m³ this is to be provided through the proposed cellular attenuation crates.

Block F1:

To attenuate surface water at source and reduce the risk of downstream flooding it is proposed that Building F1 will use of blue roofs, high level podium attenuation and a below ground attenuation tank. The approximate volume of attenuation is $185 \, \mathrm{m}^3$. It is proposed that controls will be used on the blue roofs and high level podium to ensure that all attenuation is fully utilised. The surface water drainage network will drain via gravity to the northeast of the building into a demarcation chamber restricting the discharge rate to 1.25l/s which is to be controlled via a hydrobrake, prior to discharging to the Thames Water combined sewer. It is proposed that a new connection will be made to the southeast corner of the building, branching into the Thames Water combined water sewer in Aberfeldy Street between manholes TWMH4313 & TWMH4312.

Block H1/H2 & H3:

The proposed surface water drainage strategy for the buildings H1&H2 and H3 has been made sustainable through the use of two below ground attenuation tanks (one attenuation tank serving buildings H1&H2 and one attenuation tank serving building H3) and blue/green roof areas to attenuate surface water at source and reduce the risk of downstream flooding.

The proposed surface water drainage network for buildings H1&H2 will drain via gravity to the east of the buildings into a demarcation chamber restricting the discharge rate to 1.5l/s which is to be controlled via a hydrobrake, prior to discharging to the Thames Water combined sewer. The approximate volume of attenuation for buildings H1&H2 is 161m³, of which 49m³ is provided through the blue roof and 112m³ is provided through the below ground cellular attenuation crates.

The same strategy is applied to Building H3 which will discharge surface water via gravity to the west of the building into a demarcation chamber restricting the discharge rate to 1.25l/s which is to be controlled via a hydrobrake, prior to discharging to the Thames Water combined sewer. The approximate volume of attenuation for building H3 is 135m³, of which 24m³ is provided through the blue roof and 111.2m³ is provided through the below ground cellular attenuation crates.

Buildings H1&H2 and H3 will discharge surface water via two new separate connections into Thames Water combined sewer in Aberfeldy Street (TWMH4215).

The proposed new connections are subject to a CCTV survey which will survey the line, level and condition of the existing sewers. If this survey identifies any available existing connections in those locations there may be an opportunity to reuse. This will be explored during detailed design.

To achieve the proposed discharge rates 6.25l/s it is required to attenuate an approximate volume of 896m³.

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Phase B Strategy - Outline Planning Application

The proposed surface water strategy for the phase B has been developed to utilise sustainable drainage systems (SuDS) to attenuate surface water at source and reduce the risk of downstream flooding of the Thames Water sewer network. The scheme that has been developed to utilise a combination of blue roofs, high level podium attenuation and attenuation tanks.

The proposed strategy includes a total of three new connections to the existing Thames Water combined sewer network. These are outlined below:

- One connection to the Thames Water combined sewer network in Leven Road (TWMH3605), through a new connection serving the adjacent Block A1/A2 receiving a restricted discharge rate of 1.5l/s.
- One connection to the Thames Water combined sewer network in Abbott Road (TWMH3517 to TWMH2536), through a new connection serving Block A3, B1/B2 & B4 receiving a total restricted discharge rate of 3.5l/s.
- One connection to the Thames Water combined sewer network in Abbott Road (TWMH3516), through a new connection serving Blocks B3 and B5 receiving a total restricted discharge rate of 2.3l/s.

The proposed new connections are subject to a CCTV survey which will survey the line, level and condition of the existing sewers. If this survey identifies any available existing connections in those locations there may be an opportunity to reuse. This will be explored during detailed design.

To achieve the proposed discharge rates 7.3l/s it is required to attenuate an approximate volume of 862m³.

Phase C Strategy - Outline Planning Application

The proposed drainage strategy for Phase C is similar to that of Phase B. It is proposed that surface water will be attenuated through the use of SuDS to minimise the likelihood of downstream flooding. It is proposed that the primary source of attenuation for Phase C will be below ground attenuation tanks with further attenuation to be provided via blue roofs and high levels podium attenuation.

It is proposed that surface water from the Phase C will flow via gravity to the east of this phase where a new connection to the Thames Water network in Ettrick Street (TWMH4303), will be made. This is subject to a CCTV survey which will survey the line, level and condition of the existing sewer. If this survey identifies any available existing connections in this location there may be an opportunity to reuse. This will be explored during detailed design.

Each block shall attenuate and restrict flows separately before connecting into TWMH4303, the below summaries the proposed discharge rates and required attenuation for each block within phase C;

- Block C1/C2/C3/C4 shall restrict discharge rate to 1.5l/s requiring a total 651m³ attenuation of which 425m³ is to be provided through below ground cellular attenuation crates and 238m³ provided via blue roofs and high levels podium attenuation.
- Block C5 & C6 have been designed to have a shared flow control structure limiting discharge to 1l/s with attenuation however split both buildings to receive 10m³ attenuation provided through below ground cellular attenuation crates. Flows from Blocks C5 and C6 are to be conveyed into a combined running along Ettrick Street to the east before discharging into TWMH4303.
- Block E1/E2/E3 is to restrict discharge rate to 1.5l/s requiring a total 563m³ attenuation of which 400.4m³ is to be provided via below ground cellular attenuation crates and 162m³ provided via blue roofs and high levels podium attenuation.



The Phase C development shall therefore discharge at a maximum 4l/s for the 1:100 year plus 40% climate change event, this flow is all conveyed into the Thames Water Manhole TWMH4303 in Ettrick Street. The total amount of attenuation to be provided for this phase is 1233m³.

Phase D Strategy - Outline Planning Application

The proposed surface water drainage strategy for the building Phase D has been made sustainable through the use of a below ground attenuation tank and blue roofs and high levels podium attenuation

The proposed surface water strategy for the building Phase D is to discharge surface water via gravity to the southeast of Phase D into Thames Water combined water sewer in Ettrick Street (TWMH4302) via a new connection. This is subject to a CCTV survey which will survey the line, level and condition of the existing sewer. If this survey identifies any available existing connections in this location there may be an opportunity to reuse. This will be explored during detailed design.

Surface water discharge from the site is to be restricted to 1.5l/s which is to be controlled via a hydrobrake on a demarcation manhole prior to discharging into Thames Water combined water sewer. The approximate volume of attenuation for Phase D is 576m³, of which 490m³ is to be provided via below ground attenuation crates and 87m³ provided via and blue roof attenuation.

For full drainage strategy drawings refer to the appendices.

2.1.4 Proposed Discharge Rates Summary

The table below shows the volume of surface water attenuation required to suit a 1 in 100-year storm event + 40% climate change. A breakdown of the proposed discharge rates and required attenuation volumes is shown in Table 1.

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	Storm Event	Proposed Discharge Rate	Required Surface Water Attenuation
Phase A Blocks I1, J1, F1, H1&H2 and H3	1 in 100 year + 40% CC	6 l/s	896m³
Phase B	1 in 100 year + 40% CC	7.3 l/s	865m³
Phase C	1 in 100 year + 40% CC	4 l/s	1231m³
Phase D	1 in 100 year + 40% CC	1.5 l/s	576m³
Total		18.8 l/s	3568m³

Table2-2: Proposed Surface Water Discharge Rates

2.1.5 Water Quality

The proposed drainage strategy manages pollution risk for the site based on a simple qualitative method as defined in the CIRIA SuDS Manual C753, consisting of an assessment of likely pollution hazard levels for the site and SuDS performance capacities:



Land use	Pollution hazard level	Total suspended solids (TSS)	Metals	Hydro- carbons
Residential roofs	Very low	0.2	0.2	0.05
Other roofs (typically commercial/ industrial roofs)	Low	0.3	0.2 (up to 0.8 where there is potential for metals to leach from the roof)	0.05
Individual property driveways, residential car parks, low traffic roads (eg cul de sacs, homezones and general access roads) and non- residential car parking with infrequent change (eg schools, offices) ie < 300 traffic movements/day	Low	0.5	0.4	0.4
Commercial yard and delivery areas, non-residential car parking with frequent change (eg hospitals, retail), all roads except low traffic roads and trunk roads/motorways¹	Medium	0.7	0.6	0.7
Sites with heavy pollution (eg haulage yards, lorry parks, highly frequented lorry approaches to industrial estates, waste sites), sites where chemicals and fuels (other than domestic fuel oil) are to be delivered, handled, stored, used or manufactured; industrial sites; trunk roads and motorways ¹	High	0.82	0.82	0.9²

Figure 2-3: Extract from CIRIA C753: Pollution Hazard Indicines

The site is predominantly roof areas and pedestrian walkways and as such, the site has a Low Pollution hazard level. Surface water run-off will be managed using a range of SuDS detailed previously that will offer water quality benefits.

The car parking a ground level is covered and therefore will be discharged to the foul network.

SuDS bio-retention planters and green roofs will provide pollution control as they assit with removing heavy metals and hydrocarbons from surface water run-off.

2.1.6 Amenity, Bio-diversity and Multi-functional benefits

The proposed drainage strategy offers a number of multifaceted benefits across amenity, biodiversity and other areas. Blue/green roofs provide a positive impact on amenity for the site and green roofs and SuDS bio-retention areas help to improve and increase bio-diversity. As discussed in the section above, the SuDS bio-retention planters and green roofs in particular in addition to other SuDS features help to improve water quality from the site.

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2.2 Foul Water Drainage

2.2.1 Drainage Design Parameters

The below-ground foul drainage system will be designed to Sewers for Adoption 7th Edition, BS EN 752 Parts 3 and 4, and the Building Regulations Document H where appropriate.

2.2.2 Proposed Foul Water Drainage Strategy

Due to size and phasing of the development, it is proposed that foul drainage from the site will be split into 10 individual outfalls into the Thames Water combined network. Splitting the foul discharge from the site is important due to the potential increase in flow, reducing the impact on the existing Thames Water combined drainage network.

The proposed foul water drainage strategy for the site involves the MEP engineer's coordination of the superstructure drainage up until it exits the building and enters the below ground drainage network. A below ground drainage network of pipes and manholes will collect the foul water discharge from the buildings and convey to a demarcation chamber, before discharging via gravity to the existing Thames Water combined water sewers within the site or surrounding the site. This will be coordinated during detailed design.

The proposed strategy includes various connections to the existing Thames Water combined sewer network. These are outlined below.

As phase A is divided into 3 different locations it is proposed that Blocks I1, J1, F1, H1&H2 and H3 to drain separately into the closest Thames Water combined water sewer network. Therefore five connections to the Thames Water combined water sewer network are proposed for phase A:

- For the building I1 it is proposed that a new connection will be made to the northwest corner of the building into the Thames Water combined water network in Blair Street (TWMH7303);
- It is proposed that building J1 to discharge foul water into Thames Water combined water sewer in Leven Road (TWMH3602) via a new connection;
- It is proposed that a new connection will be made to the southeast corner of the building F1 into the Thames Water combined water sewer in Aberfeldy Street (TWMH4313-TWMH4312); and
- Buildings H1&H2 and H3 will discharge foul water via two new separate connections into Thames Water combined sewer in Aberfeldy Street (TWMH4215).

The proposed strategy for phase B includes a total of three connections to the existing Thames Water combined sewer network. These are outlined below:

- One connection to the Thames Water combined sewer network in Leven Road (TWMH3605), through a new connection serving building A1/A2;
- One connection to the Thames Water combined sewer network in Abbott Road (TWMH3517 to TWMH2536), through a new connection serving buildings A3, B1/B2 and B4;
- One connection to the Thames Water combined sewer network in Abbott Road (TWMH3516), through a new connection serving building B3/B5.

It is proposed that foul water from the Phase C will flow via gravity to the east of this phase where a new connection to the Thames Water network in Ettrick Street (TWMH4303) will be made. This will be serving the buildings C1/C2/C3/C4, C5, C6 & E1/E2/E3.



The proposed foul water strategy for the building Phase D is to discharge foul water via gravity to the southeast of the phase D into Thames Water combined water sewer in Ettrick Street (TWMH4302) via a new connection.

The proposed new connections are subject to a CCTV survey which will survey the line, level and condition of the existing sewers. If this survey identifies any available existing connections in those locations there may be an opportunity to reuse. This will be explored during detailed design.

The discharge locations and foul water strategy will be confirmed during detailed design and a Section 106 drainage connection application for each connection will be submitted at the construction stage to Thames Water for formal approval of the proposed connections arrangement.

2.2.3 Proposed Foul Water Discharge Rates

Based on the most recent accommodation schedule (as at 17.09.21), the peak foul water discharge rate from the site will be in the region of 75l/s. This proposed discharge rate has been calculated in accordance with BS EN 12056-2, however, this will be confirmed by Meinhardt's MEP engineer during detailed design.

Thames Water have been contacted and have confirmed they have sufficient capacity in their network to accept the proposed flows from the development (surface water and foul water).

2.3 Proposed Combined Water Flow Rates

The proposed combined water discharge rates for the site are outlined in Table 1.

Contributing Area (ha)	Proposed Surface Water Discharge Rate [1 in 100 year storm + 40% CC] (I/s)	Proposed Peak Foul Water Discharge Rate (I/s)	Proposed Combined Peak Discharge Rate (I/s)	Reduction compared to Existing Combined Discharge Rate
3.00	18.8	75.58	94.63	65%

Table 1: Proposed Combined Water Discharge Rates

The proposed discharge rates will be confirmed during detailed design.

2.4 Site Wide Foul Water Drainage Coordination

The proposed foul water drainage strategy for the site involve coordination with Meinhardts MEP engineer's to coordination the superstructure drainage up until it enters the below ground drainage network. A below ground drainage network of pipes and manholes will collect the foul water discharge from the buildings before discharging via gravity into the Thames Water combined sewer located in the surrounding roads.

Any ground floor or basement level foul water drainage that can't be drained by gravity will be routed to private basement foul water pump chambers which will lift foul water from the basements into the internal drainage network before draining via gravity into the external below ground drainage network.

2.5 Operations and Maintenance

2.5.1 Pipes (Including Oversized)

2.5.1.1 Location and Description

Pipes are proprietary products and the materials can vary across the site and as such where used the manufacturer's recommendations should be followed. Regardless of the product used, the pipes will be fully compliant with the Meinhardt drainage specification.

Aberfeldy Village, London Masterplan, Below Ground Drainage Strategy



2.5.1.2 Operation

They are intended to be dry except for during rainfall events. These have been designed to be self-cleansing for smaller diameter pipes, and for larger diameters the risk is reduced due to the overall pipe size.

Access for maintenance is provided through access chambers, manholes, rodding plates and rodding eyes.

2.5.1.3 Inspection and Maintenance Regime

Regular inspection and maintenance is important to identify areas which may have been obstructed/clogged and may not be draining correctly thus exposing the development to a greater level of flood risk. Maintenance responsibility for the pipes should be placed with Ecoworld.

Sediment/material removal should be undertaken in consultation with the environmental regulator to confirm appropriate protocols, as run-off is taken from potentially contaminated areas such as car parks/service yards.

Maintenance Schedule	Required Action	Frequency
Monitoring (to be undertaken more	Initial inspection should be provided as post construction CCTV survey.	N/A
regularly within the first year of operation and adjusted as required)	Inspect for evidence of poor operation via water level in chambers. If required, take remedial action.	3-monthly, 48 hours after large storms.
Occasional maintenance	Check and remove large vegetation growth near pipe runs.	6 monthly
Remedial actions	Rod through poorly performing runs as initial remediation.	As required.
	If continued poor performance jet and CCTV survey poorly performing runs.	As required.
	Seek advice as to remediation techniques suitable for the type of performance issue and location.	As required If above does not improve performance.



2.5.2 Green/Blue Roofs, Location and Description

A green/blue roof specialist will be required at later design stages.

2.5.2.1 Inspection and Maintenance Regime

Regular inspection and maintenance is important to identify areas which may have been obstructed/clogged and may not be draining correctly thus exposing the development to a greater level of flood risk. Maintenance responsibility for the pipes should be placed with Ecoworld.

Maintenance Schedule	Required Action	Typical Frequency
	Inspect all components including soil substrate, vegetation, drains, irrigation systems (if applicable), membranes and roof structure for proper operation, integrity of waterproofing and structural stability	Annually and after severe storms
Regular inspections	Inspect soil substrate for evidence of erosion channels and identify and sediment sources	Annually and after severe storms
	Inspect drain inlets to ensure unrestricted runoff from the drainage layer to the conveyance or roof drain system	Annually and after severe storms
	Remove debris and litter to prevent clogging of inlet drains and interference with plant growth	Six monthly and annually or as required
	During establishment (ie. Year one), replace dead plans as required	Monthly (but usually responsibility of manufacturer)
	Post establishment, replace dead plants as required (where >5% of coverage)	Annually (in autumn)
Regular maintenance	Remove fallen leaves and debris from deciduous plant foliage	Six monthly and annually or as required
	Remove nuisance and invasive vegetation, including weeds	Six monthly and annually or as required
	Mow grasses, prune shrubs and manage other planting (if appropriate) as required - clippings should be removed and not allowed to accumulate	Six monthly and annually or as required
Remedial Actions	If erosion channels are evident, these should be stabilised with extra soil substrate similar to the original material and sources of erosion damage should be identified and controlled	As required
	If drain inlet has settled, cracked or moved, investigate and repair as appropriate	As required

Aberfeldy Village, London Masterplan, Below Ground Drainage Strategy



2.5.3 Bioretention Systems

2.5.3.1 Location and Description

Bio-retention systems (including rain gardens) are shallow landscaped depressions can reduce runoff rates and volumes, and treat pollution through the use of engineered soils and vegetation. They are particularly effective in delivering interception and can also provide:

- Attractive landscape features that are self-irrigating and fertilizing
- Habitat and biodiversity
- Cooling of the local microclimate due to evapotranspiration.

Bio-retention systems have been specified to be used in various privately managed public spaces throughout the site.

2.5.3.2 Operation

It has been concluded in literature (Dalrymple, 2013) that bio-retention systems will typically require approximately 2.5 times more maintenance than typical landscaped designs.

Maintenance schedule	Required Action	Typical Frequency
	Inspect infiltration surfaces for silting and ponding, record de-watering time of the facility and assess standing water levels in underdrain (if appropriate) to determine if maintenance is necessary)	Quarterly
Regular inspections	Check operation of underdrains by inspection of flows after rain	Annually
	Assess plants for disease infection, poor growth, invasive species etc and replace if necessary	Quarterly
	Inspect inlets and outlets for blockage	Quarterly
	Remove litter and surface debris and weeds	Quarterly (or more frequently for tidiness or aesthetic reasons)
Regular maintenance	Replace and plants to maintain planning density	As required
	Remove sediment, litter and debris build-up from around inlets or from forebays	Quarterly or biannually
Occasional maintenance	Infill nay holes or scour in filter medium, improve erosion protection of required	As required
maintenance	Repair minor accumulations of silt by raking away surface mulch	As required
Remedial actions	Remove and replace filter medium and vegetation above	As required but likely to be > 20 years



2.5.4 Geocellular units

2.5.4.1 Location and Description

Geocellular units are proprietary products and therefore manufacturer's specific recommendations should also be taken in to consideration above what has been prepared in this document. Additionally, different manufacturers may have different connection types and arrangements which will need to be taken in to consideration.

2.5.4.2 Operation

The geocellular units, along with permeable paving, are intended to attenuate the discharge from the site up to and including the 1 in 100 year plus 40% climate change event.

Access for maintenance has been provided through inspection chambers.

2.5.4.3 Inspection and Maintenance Regime

Regular inspection and maintenance is important for the effective operation of geocellular units as designed. As the feature is buried a regularly inspection regime is very important to ensure the correct functionality of the surface water drainage network. Maintenance responsibility for the geocellular units and their surrounding areas should be placed with Ecoworld.

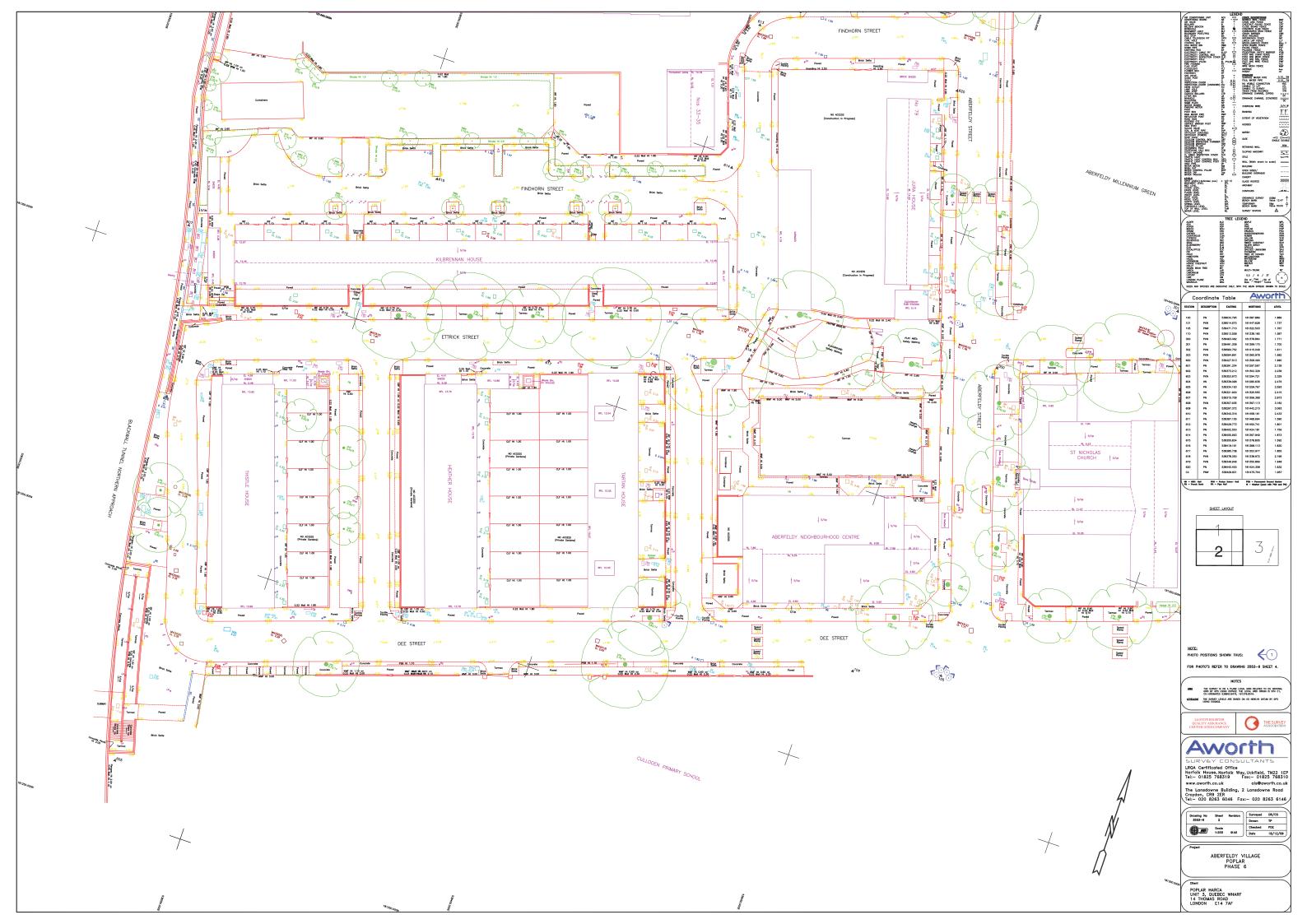
Sediment\material removal should be undertaken in consultation with the environmental regulator to confirm appropriate protocols; especially where run-off is taken from potentially contaminated areas such as car parks/service yards.

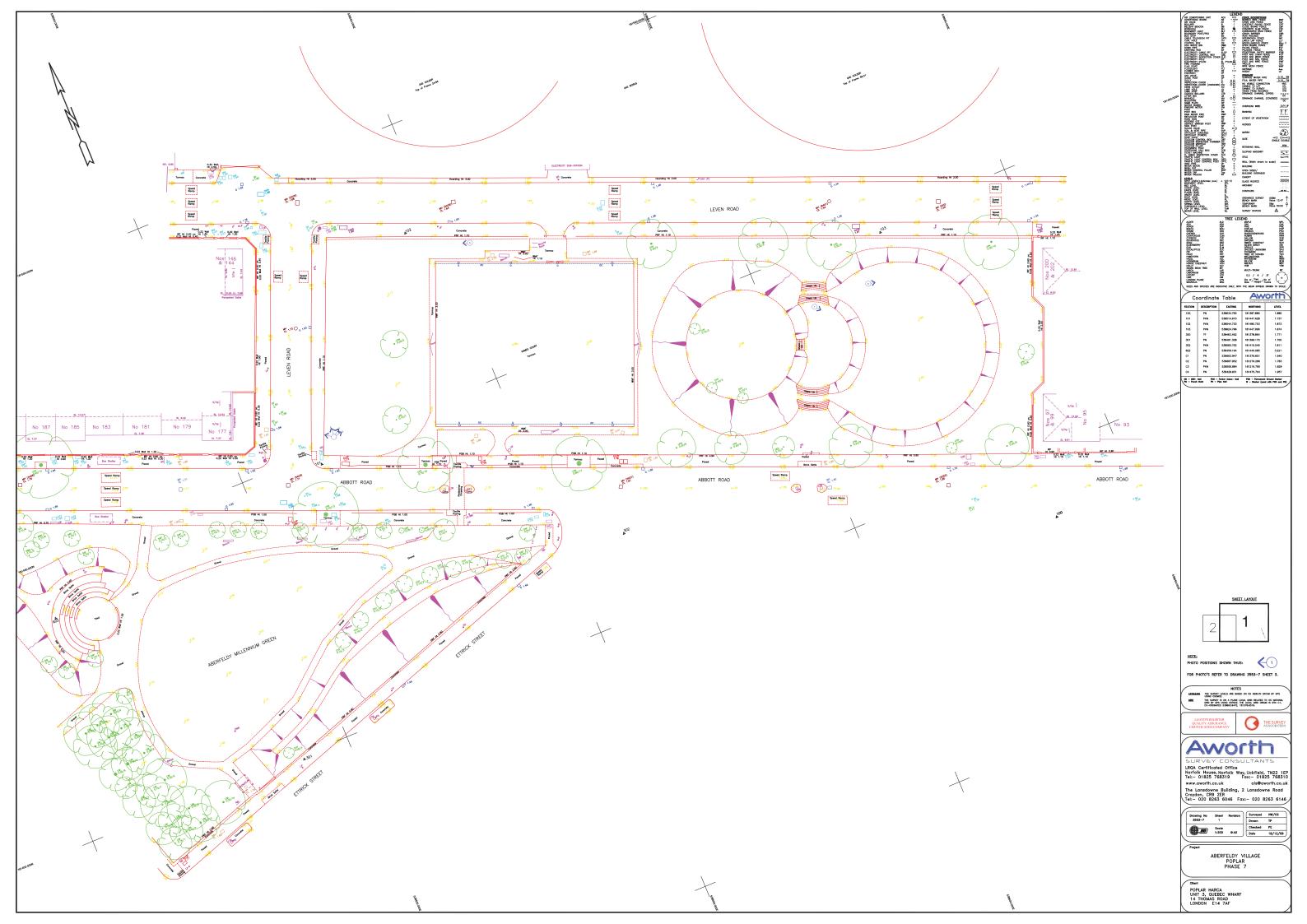
Maintenance Schedule	Required Action	Frequency
Monitoring (to be undertaken more regularly within the first year of operation and adjusted as required)	Inspect inlets, outlets and overflows for blockages, and clear if required. If faults persist jetting and CCTV survey may be required.	Monthly and after large storms.
	Check penstocks and other mechanical devices (if present).	Half yearly.
	Inspect ventilation cowl (if present)	Monthly and after large storms.
Regular maintenance\inspection	Inspect and identify any areas that are not operating correctly. If required, take remedial action.	Monthly for 3 months, then six monthly
	Debris removal from catchment surface (where may cause risks to performance)	Monthly
	Where rainfall infiltrates into blocks from above, check surface of filter for blockage by silt, algae or other matter. Remove and replace surface infiltration medium as necessary.	Monthly (and after large storms)
	Remove sediment from pre-treatment structures	Annually (or as required after heavy rainfall events)
Remedial actions	Repair/rehabilitation of inlets, outlet, overflows and vents.	As required.

Aberfeldy Village, London Masterplan, Below Ground Drainage Strategy

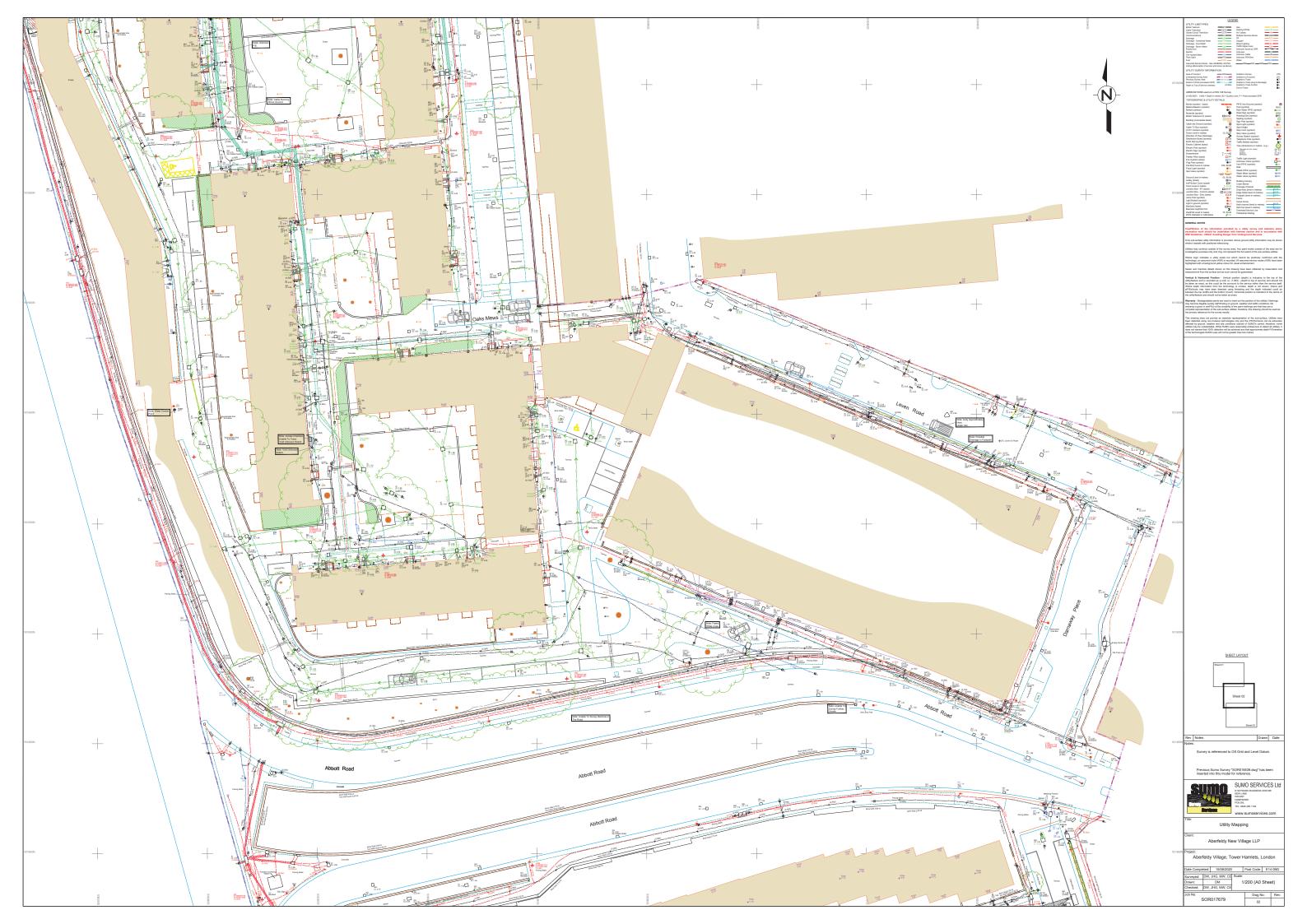


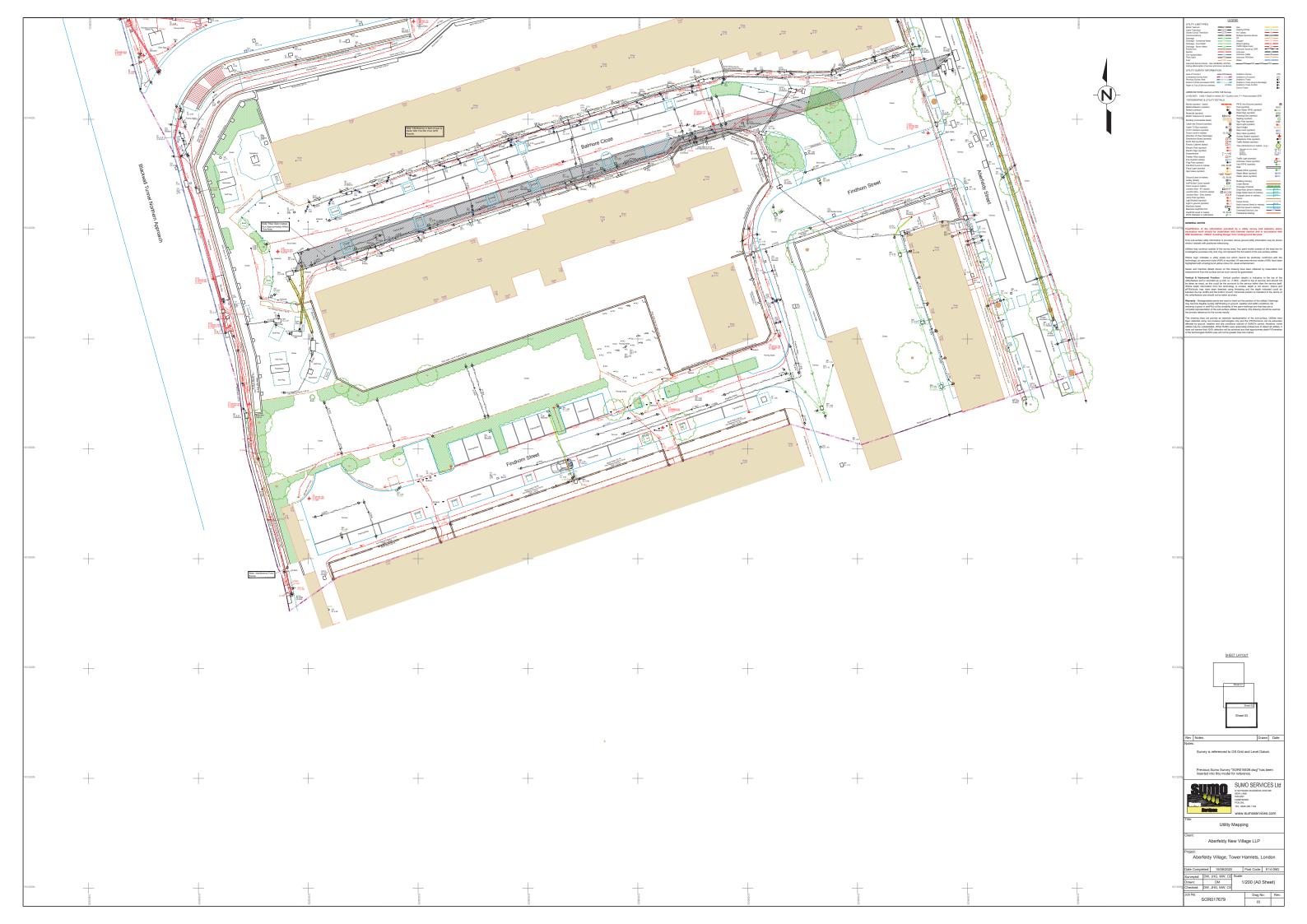
Appendix A – Topographical & Utility Surveys

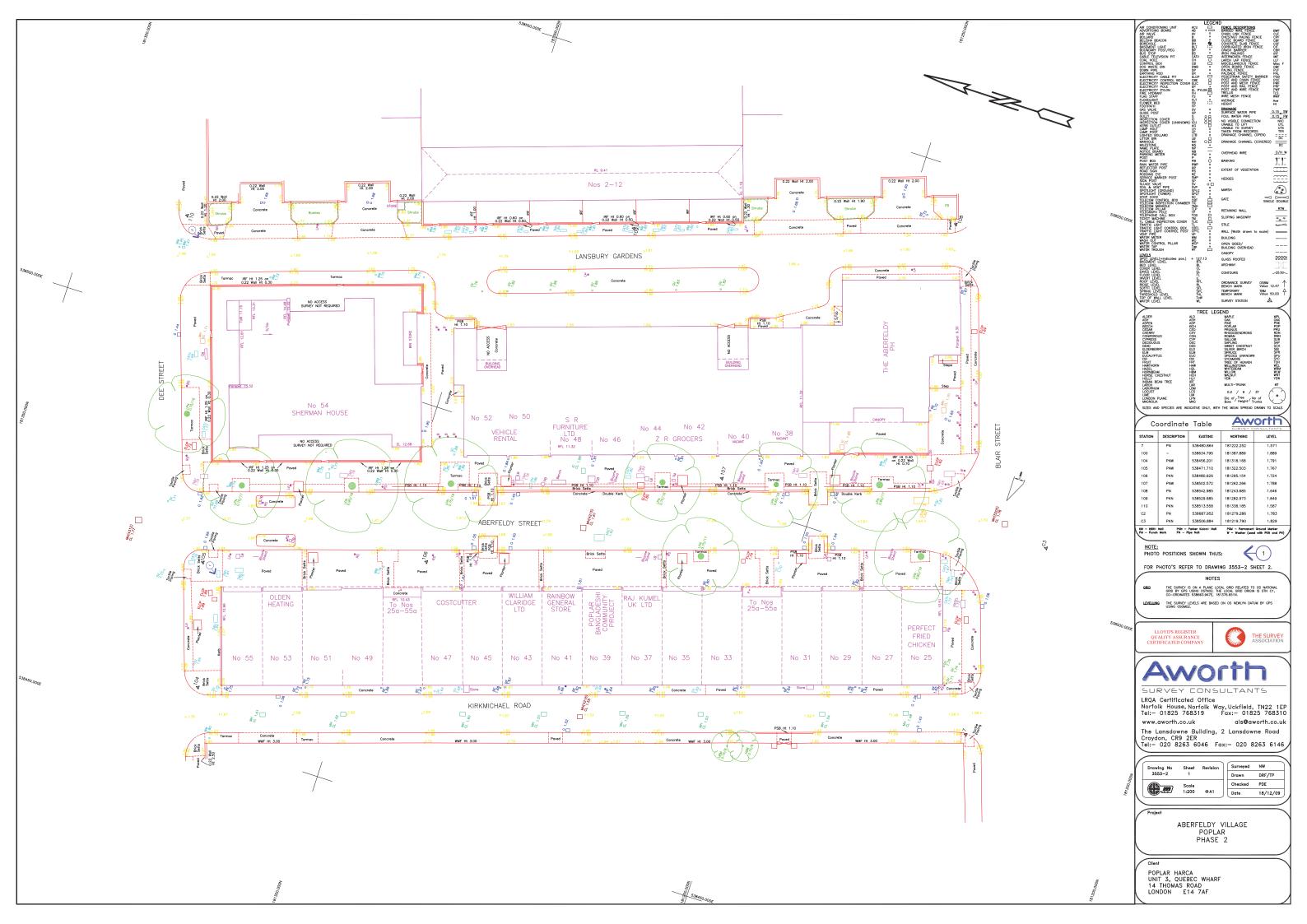
















Search address supplied: Aberfeldy Village, Aberfeldy Street, London, London, UK,

Dear Sir / Madam

An Asset Location Search is recommended when undertaking a site development. It is essential to obtain information on the size and location of clean water and sewerage assets to safeguard against expensive damage and allow cost-effective service design.

The following records were searched in compiling this report: - the map of public sewers & the map of waterworks. Thames Water Utilities Ltd (TWUL) holds all of these.

This searchprovides maps showing the position, size of Thames Water assets close to the proposed development and also manhole cover and invert levels, where available.

Please note that none of the charges made for this report relate to the provision of Ordnance Survey mapping information. The replies contained in this letter are given following inspection of the public service records available to this company. No responsibility can be accepted for any error or omission in the replies.

You should be aware that the information contained on these plans is current only on the day that the plans are issued. The plans should only be used for the duration of the work that is being carried out at the present time. Under no circumstances should this data be copied or transmitted to parties other than those for whom the current work is being carried out.

Thames Water do update these service plans on a regular basis and failure to observe the above conditions could lead to damage arising to new or diverted services at a later date.

Contact Us

If you have any further queries regarding this enquiry please feel free to contact a member of the team on 0845 070 9148, or use the address below:

Thames Water Utilities Ltd Property Searches PO Box 3189 Slough SL1 4WW

Email: searches@thameswater.co.uk

Web: www.thameswater-propertysearches.co.uk



Waste Water Services

Please provide a copy extract from the public sewer map.

The following quartiles have been printed as they fall within Thames' sewerage area:

TQ3881NE TQ3881SW TQ3881NW TQ3881SE

Enclosed is a map showing the approximate lines of our sewers. Our plans do not show sewer connections from individual properties or any sewers not owned by Thames Water unless specifically annotated otherwise. Records such as "private" pipework are in some cases available from the Building Control Department of the relevant Local Authority.

Where the Local Authority does not hold such plans it might be advisable to consult the property deeds for the site or contact neighbouring landowners.

This report relates only to sewerage apparatus of Thames Water Utilities Ltd, it does not disclose details of cables and or communications equipment that may be running through or around such apparatus.

The sewer level information contained in this response represents all of the level data available in our existing records. Should you require any further Information, please refer to the relevant section within the 'Further Contacts' page found later in this document.

For your guidance:

- The Company is not generally responsible for rivers, watercourses, ponds, culverts or highway drains. If any of these are shown on the copy extract they are shown for information only.
- Any private sewers or lateral drains which are indicated on the extract of the public sewer map as being subject to an agreement under Section 104 of the Water Industry Act 1991 are not an 'as constructed' record. It is recommended these details be checked with the developer.

Clean Water Services

Please provide a copy extract from the public water main map.

The following quartiles have been printed as they fall within Thames' water area:

TQ3881NE TQ3881SW



TQ3881NW TQ3881SE

Enclosed is a map showing the approximate positions of our water mains and associated apparatus. Please note that records are not kept of the positions of individual domestic supplies.

For your information, there will be a pressure of at least 10m head at the outside stop valve. If you would like to know the static pressure, please contact our Customer Centre on 0800 316 9800. The Customer Centre can also arrange for a full flow and pressure test to be carried out for a fee.

For your guidance:

- Assets other than vested water mains may be shown on the plan, for information only.
- If an extract of the public water main record is enclosed, this will show known public water mains in the vicinity of the property. It should be possible to estimate the likely length and route of any private water supply pipe connecting the property to the public water network.

Payment for this Search

A charge will be added to your suppliers account.



Further contacts:

Waste Water queries

Should you require verification of the invert levels of public sewers, by site measurement, you will need to approach the relevant Thames Water Area Network Office for permission to lift the appropriate covers. This permission will usually involve you completing a TWOSA form. For further information please contact our Customer Centre on Tel: 0845 920 0800. Alternatively, a survey can be arranged, for a fee, through our Customer Centre on the above number.

If you have any questions regarding sewer connections, budget estimates, diversions, building over issues or any other questions regarding operational issues please direct them to our service desk. Which can be contacted by writing to:

Developer Services (Waste Water) Thames Water Clearwater Court Vastern Road Reading RG1 8DB

Tel: 0800 009 3921

Email: developer.services@thameswater.co.uk

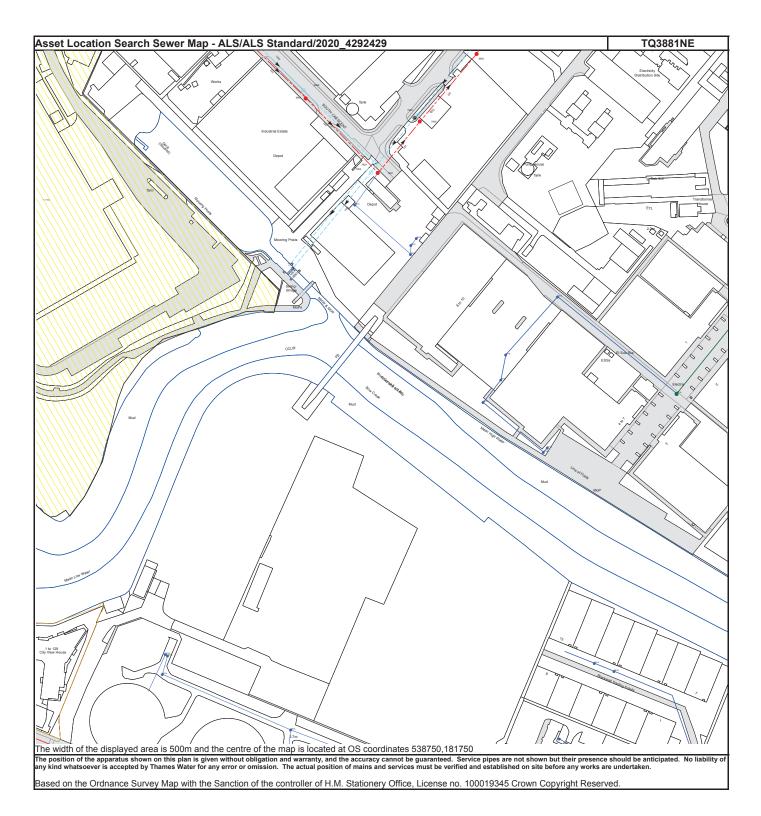
Clean Water queries

Should you require any advice concerning clean water operational issues or clean water connections, please contact:

Developer Services (Clean Water) Thames Water Clearwater Court Vastern Road Reading RG1 8DB

Tel: 0800 009 3921

Email: developer.services@thameswater.co.uk



<u>Thames Water Utilities Ltd.</u> Property Searches, PO Box 3189, Slough SL1 4W, DX 151280 Slough 13

T 0845 070 9148 E searches@thameswater.co.uk I www.thameswater-propertysearches.co.uk

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NB. Levels quoted in metres Ordnance Newlyn Datum. The value -9999.00 indicates that no survey information is available

Manhole Reference	Manhole Cover Level	Manhole Invert Level
85AB	n/a	n/a
85AC	n/a	n/a
951A	n/a	n/a
951B	n/a	n/a
8904	n/a	n/a
8903	n/a	n/a
781A	n/a	n/a
7802	n/a	n/a
7803	n/a	n/a
7801	n/a	n/a
781B	n/a	n/a
781C	n/a	n/a
781D	n/a	n/a
871C	n/a	n/a
871D	n/a	n/a
871E	n/a	n/a
871B	n/a	n/a
871A	n/a	n/a
881A	n/a	n/a
971A	n/a	n/a
651A	n/a	n/a
6902	n/a	n/a
6901	n/a	n/a
7902	n/a	n/a
7905	n/a	n/a
551A	n/a	n/a
551C	n/a	n/a
551B	n/a	n/a

The position of the apparatus shown on this plan is given without obligation and warranty, and the accuracy cannot be guaranteed. Service pipes are not shown but their presence should be anticipated. No liability of any kind whatsoever is accepted by Thames Water for any error or omission. The actual position of mains and services must be verified and established on site before any works are undertaken.

Thames Water Utilities Ltd, Property Searches, PO Box 3189, Slough SL1 4W, DX 151280 Slough 13

T 0845 070 9148 E searches@thameswater.co.uk | www.thameswater-propertysearches.co.uk

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NB. Levels quoted in metres Ordnance Newlyn Datum. The value -9999.00 indicates that no survey information is available

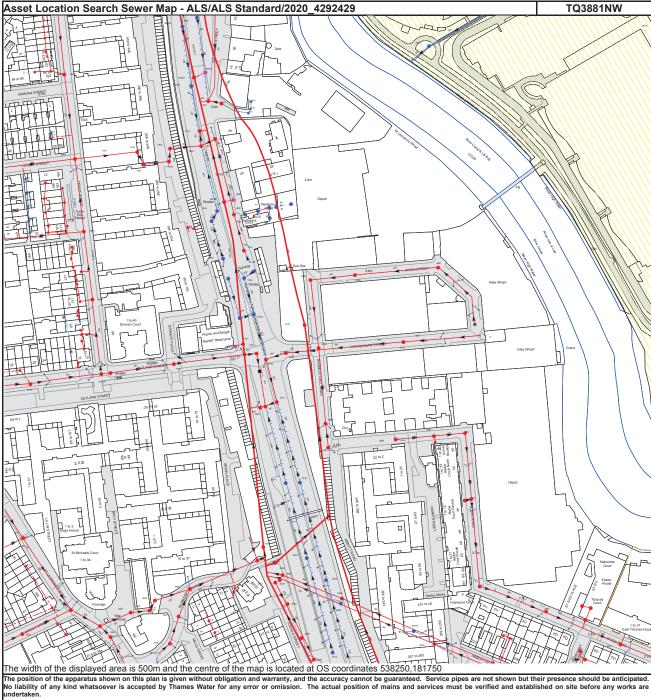
[T	
Manhole Reference	Manhole Cover Level	Manhole Invert Level
3402	1.92	-3.79
3403	1.94	54
2417 141A	3 n/a	1.5 n/a
2424	2.32	n/a
141G 411H	n/a n/a	n/a n/a
4203	1.7	48
4204	1.79	7
4202 4201	1.71 1.7	9 94
42DH	n/a	n/a
42DI 42DJ	n/a n/a	n/a n/a
42EA	n/a	n/a
4216	1.57	-1.33
42EE 4215	n/a 1.61	n/a -2.24
42EG	n/a	n/a
42ED 43DB	n/a n/a	n/a n/a
33CH	n/a	n/a
4301A	1.77	-2.82
43DE 431E	n/a n/a	n/a n/a
43DD	n/a	n/a
43DF 4319	n/a 1.76	n/a -1.28
43DG	n/a	n/a
44DB	n/a	n/a n/a
44DA 44CI	n/a n/a	n/a n/a
44DC	n/a	n/a
44DD 44CH	n/a n/a	n/a n/a
44CJ	n/a	n/a
3432 4420	1.68 1.59	-1.72 -3.16
4419	1.7	-3.27
4408	1.75	-3.45
3405 4407	1.72 1.97	.13 -3.55
4401	1.76	05
3404 3222	1.67 2.36	33 .55
32CG	n/a	n/a
42EC	n/a	n/a
33EE 4313	n/a 2.04	n/a -1.04
43DI	n/a	n/a
33ED 33EC	n/a n/a	n/a n/a
33EB	n/a	n/a
4312 33EA	1.73 n/a	-2.54 n/a
33DJ	n/a	n/a
431D	n/a	n/a
431C 33CE	n/a n/a	n/a n/a
4303	n/a	n/a
4302 431B	n/a n/a	n/a n/a
33DB	n/a	n/a
33DC	n/a n/a	n/a n/a
431A 33DD	n/a n/a	n/a n/a
3016	4.41	-1.42
3015 3014	4.08 3.45	-1.55 -1.74
3010	n/a	n/a
3023 3005	4.25 n/a	1.24 n/a
3009	3.98	1.27
3008	4.06	2.68
3007 3006	4.16 6.19	-1.23 2.89
2422	2.26	-4.27
2406 2409	2.7 2.99	1.83 2.3
2409	n/a	n/a
2304	2.49	1.07
2420 2303	3.36 2.35	1.54 .8
2305	2.66	1.02
2301 3306	2.38 2.49	.73 1.72
3310	2.57	.74
3406	2.76	1.11
3401	3.04	-8.94

Mainton Water Even Mainton M	Manhole Reference	Manhole Cover Level	Manhole Invert Level
3201			
2.35 4.07		-	
10			7
10	33CD	n/a	n/a
10			
1988 1988			
1988 1988			7
10			
1916		n/a	n/a
2012			
2112	2102	4.37	1.67
1912			
1912	3112		
1913 1916			
1311C			
118			
111A			
Mile	311A	n/a	n/a
Main			
Main			7
1118			
411			
111	4111	n/a	n/a
4103			
4011	4103	1.85	11
1912			
128D			
128E			
22CE			
128F			
128F			
22BI n/a n/a 22CA n/a n/a 22CB n/a n/a 22CC n/a n/a 22CC n/a n/a 21CE n/a n/a 21CD n/a n/a 21CD n/a n/a 21CC n/a n/a 2201 2.35 1.21 2202 3.7 1.85 2204 3.93 2.12 2204 2.97 .77 2212 2.64 1.93 3218 2.85 1.21 3217 2.74 1.64 3201 2.74 1.64 3203 2.47 -1.25 12EB n/a n/a 12EB	12BF	n/a	n/a
22EJ n/a n/a 22CB n/a n/a 22CC n/a n/a 22CC n/a n/a 22CC n/a n/a 22CC n/a n/a 21CE n/a n/a 21CC n/a n/a 2203 5.2 2.35 21CC n/a n/a 2204 3.93 2.12 2204 3.93 2.12 2201 2.97 .77 2212 2.64 1.93 3218 2.85 1.21 3217 2.94 .53 3217 2.94 .53 3219 2.74 1.64 3201 2.44 -8.63 3201 2.44 -8.63 3203 2.47 -1.25 12EB n/a n/a 12H n/a n/a 12H 6.7 4.86 12H			
22CB			
22CC			
21CE			
21CD			
2203 5.2 2.35 1/a 1/			
2202 3.7 1.85 2.12 2.204 3.93 3.212 2.201 2.97 .77	2203	5.2	2.35
2204 3.93 2.12 2.97 2.77 2.77 2.212 2.64 1.93 3.218 2.285 1.21 3.218 3.219 2.74 3.53 3.219 3.219 2.74 3.63 3.201 2.44 -8.63 3.203 2.47 -1.25 -1.			
2212 2.64 1.93 3218 3.218 2.85 1.21 3217 3219 2.74 1.64 3201 3.201 3.24 -8.63 3.204 3.204 3.204 -8.33 3.203 2.47 -1.25 3.208 1.21 3.208 3.203 2.47 -1.25 3.208 3.2			
3218 2.85 1.21 3217 2.94 5.53 3219 2.74 1.64 3201 2.44 8.63 3204 2.34 8.63 3203 2.47 1.25 1.26 1.27 1.25 1.25 1.25 1.26 1.27 1.27 1.28 1.21 1.22 1.23 1.24			
3217 2.94 5.53 3.219 3.219 3.219 3.201 3.201 2.44 8.63 8.63 3.204 3.234 7.83 3.233 3.247 7.1.25 7.125 7.			
3201 2.44 -8.63 3204 3204 2.34 83 3203 2.47 -1.25 7.12	3217	2.94	.53
3204 2.34 83 3203 32.47 -1.25 3204 3203 32.47 -1.25 3204 3203 32.47 -1.25 3204 3208 3			
12EB n/a n/a 12EA n/a n/a 121F 5.7 4.88 121K 5.65 4.88 121T 5.98 3.89 121J n/a n/a 121G 5.7 4.55 12DJ n/a n/a 121E n/a n/a 121H n/a n/a 121D 5.7 3.04 121D 5.7 3.04 121D 6.31 4.9 121C 5.99 3.08 121R 6.17 4.07 12DH n/a n/a 12FH n/a n/a 12EJ n/a n/a 12EJ n/a n/a 12CA n/a n/a 12AI n/a n/a 12BA n/a n/a 12BB n/a n/a 12BC n/a n/a 12BC n/a n/a	3204	2.34	83
12EA n/a n/a 121I n/a n/a 121F 5.7 4.88 121T 5.98 3.89 121J n/a n/a 121G 5.7 4.55 12DJ n/a n/a 121E n/a n/a 121H n/a n/a 121D 5.7 3.04 121D 5.7 3.04 121D 5.7 3.04 121D 6.31 4.9 12DI n/a n/a 12DI n/a n/a 121R 6.17 4.07 12DH n/a n/a 12FH n/a n/a 12FI n/a n/a 12BJ n/a n/a 12CA n/a n/a 12AI n/a n/a 12AI n/a n/a 12BA n/a n/a 12BB n/a n/a 12BC n/a n/a			
121F 5.7 4.88 121K 5.65 4.88 121J 5.98 3.89 121J n/a n/a 121G 5.7 4.55 12DJ n/a n/a 121E n/a n/a 121H n/a n/a 121D 5.7 3.04 121D 5.7 3.04 121O 6.31 4.9 12DI n/a n/a 121C 5.99 3.08 121R 6.17 4.07 12DH n/a n/a 12FH n/a n/a 12FI n/a n/a 12BJ n/a n/a 12CA n/a n/a 12AI n/a n/a 12AJ n/a n/a 12BA n/a n/a 12BC n/a n/a 12BC n/a n/a	12EA	n/a	n/a
121K 5.65 4.88 121T 5.98 3.89 121J n/a n/a 121G 5.7 4.55 12DJ n/a n/a 121E n/a n/a 121H n/a n/a 121H n/a n/a 121D 5.7 3.04 121O 6.31 4.9 12DI n/a n/a 12DI n/a n/a 121C 5.99 3.08 121R 6.17 4.07 12DH n/a n/a 12FH n/a n/a 12FI n/a n/a 12BJ n/a n/a 12CA n/a n/a 12AI n/a n/a 12AJ n/a n/a 12BA n/a n/a 12BB n/a n/a 12BC n/a n/a			
121T 5.98 3.89 121J n/a n/a 121G 5.7 4.55 12DJ n/a n/a 121E n/a n/a 121H n/a n/a 121D 5.7 3.04 121O 6.31 4.9 12DI n/a n/a 121C 5.99 3.08 121R 6.17 4.07 12DH n/a n/a 12FH n/a n/a 12FI n/a n/a 12BJ n/a n/a 12CA n/a n/a 12AI n/a n/a 12AJ n/a n/a 12BA n/a n/a 12BB n/a n/a 12BC n/a n/a			
121G 5.7 4.55 12DJ n/a n/a 121E n/a n/a 121H n/a n/a 121D 5.7 3.04 121O 6.31 4.9 12DI n/a n/a 121C 5.99 3.08 121R 6.17 4.07 12DH n/a n/a 12FH n/a n/a 12FI n/a n/a 12BJ n/a n/a 12CA n/a n/a 12CB n/a n/a 12AJ n/a n/a 12BA n/a n/a 12BB n/a n/a 12BC n/a n/a	121T	5.98	3.89
12DJ n/a n/a 121E n/a n/a 121H n/a n/a 121D 5.7 3.04 121O 6.31 4.9 12DI n/a n/a 121C 5.99 3.08 121R 6.17 4.07 12DH n/a n/a 12FH n/a n/a 12FI n/a n/a 12BJ n/a n/a 12CA n/a n/a 12CB n/a n/a 12AI n/a n/a 12BA n/a n/a 12BB n/a n/a 12BC n/a n/a			
121H n/a n/a 121D 5.7 3.04 121O 6.31 4.9 12DI n/a n/a 121C 5.99 3.08 121R 6.17 4.07 12DH n/a n/a 12FH n/a n/a 12FI n/a n/a 12BJ n/a n/a 12CA n/a n/a 12CB n/a n/a 12AI n/a n/a 12BA n/a n/a 12BC n/a n/a 12BC n/a n/a	12DJ	n/a	n/a
121D 5.7 3.04 121O 6.31 4.9 12DI n/a n/a 121C 5.99 3.08 121R 6.17 4.07 12DH n/a n/a 12FH n/a n/a 12FI n/a n/a 12BJ n/a n/a 12CA n/a n/a 12CB n/a n/a 12AI n/a n/a 12BA n/a n/a 12BB n/a n/a 12BC n/a n/a			
12DI n/a n/a 121C 5.99 3.08 121R 6.17 4.07 12DH n/a n/a 12FH n/a n/a 12FI n/a n/a 12BJ n/a n/a 12CA n/a n/a 12CB n/a n/a 12AI n/a n/a 12BA n/a n/a 12BB n/a n/a 12BC n/a n/a	121D	5.7	3.04
121C 5.99 3.08 121R 6.17 4.07 12DH n/a n/a 12FH n/a n/a 12FI n/a n/a 12BJ n/a n/a 12CA n/a n/a 12CB n/a n/a 12AI n/a n/a 12AJ n/a n/a 12BA n/a n/a 12BC n/a n/a 12BC n/a n/a			
121R 6.17 4.07 12DH n/a n/a 12FH n/a n/a 12FI n/a n/a 12BJ n/a n/a 12CA n/a n/a 12CB n/a n/a 12AI n/a n/a 12AJ n/a n/a 12BA n/a n/a 12BB n/a n/a 12BC n/a n/a			
12FH n/a n/a 12FI n/a n/a 12BJ n/a n/a 12CA n/a n/a 12CB n/a n/a 12AI n/a n/a 12AJ n/a n/a 12BA n/a n/a 12BB n/a n/a 12BC n/a n/a	121R	6.17	4.07
12FI n/a n/a 12BJ n/a n/a 12CA n/a n/a 12CB n/a n/a 12AI n/a n/a 12AJ n/a n/a 12BA n/a n/a 12BB n/a n/a 12BC n/a n/a			
12CA n/a n/a 12CB n/a n/a 12AI n/a n/a 12AJ n/a n/a 12BA n/a n/a 12BB n/a n/a 12BC n/a n/a	12FI	n/a	n/a
12CB n/a n/a 12AI n/a n/a 12AJ n/a n/a 12BA n/a n/a 12BB n/a n/a 12BC n/a n/a			
12AI n/a n/a 12AJ n/a n/a 12BA n/a n/a 12BB n/a n/a 12BC n/a n/a			
12BA n/a n/a 12BB n/a n/a 12BC n/a n/a	12AI	n/a	n/a
12BB n/a n/a n/a 12BC n/a n/a			
· · · · · · · · · · · · · · · · · · ·	12BB	n/a	n/a
			n/a

Manhole Reference	Manhole Cover Level	Manhole Invert Level
11ED	n/a	n/a
11EC	n/a	n/a
11EB 21BE	n/a n/a	n/a n/a
11CG	n/a	n/a
11EA	n/a	n/a
21CH	n/a	n/a
21BF 11CH	n/a n/a	n/a n/a
11DJ	n/a	n/a
11CI	n/a	n/a
11CJ 21BG	n/a n/a	n/a n/a
11DA	n/a	n/a
11DB	n/a	n/a
11DI	n/a	n/a
21BH 11DC	n/a n/a	n/a n/a
11DH	n/a	n/a
21BI	n/a	n/a
11DF	n/a	n/a
11DG 21BJ	n/a n/a	n/a n/a
2110	5.27	3.03
21CA	n/a	n/a
21CB 2109	n/a 4.66	n/a 2.72
10DF	n/a	n/a
20DC	n/a	n/a
101A	n/a	n/a
20CD 10CC	n/a n/a	n/a n/a
10CI	n/a	n/a
20CI	n/a	n/a
1017	5.67	2.64
10CD 1016	n/a 5.23	n/a 2.03
10FD	n/a	n/a
20CJ	n/a	n/a
2019 10FE	4.77 n/a	1.79 n/a
11EI	n/a	n/a
11EJ	n/a	n/a
11FA	n/a	n/a
11FB 11FC	n/a n/a	n/a n/a
11FE	n/a	n/a
11FH	n/a	n/a
1102B	5.81	2.58
11EG 11EF	n/a n/a	n/a n/a
1101A	5.8	2.17
11EE	n/a	n/a
2103 02CH	4.5 n/a	2.19 n/a
12GD	n/a	n/a
12DG	n/a	n/a
12BI	n/a	n/a
12DF 12DD	n/a n/a	n/a n/a
12DC	n/a	n/a
12BH	n/a	n/a
12DB 12DA	n/a n/a	n/a n/a
12CJ	n/a	n/a
12GF	n/a	n/a
1205	n/a	n/a
12Cl 12BG	n/a n/a	n/a n/a
12CH	n/a	n/a
12CC	n/a	n/a
13DH 13DE	n/a n/a	n/a n/a
13DG	n/a n/a	n/a n/a
13DF	n/a	n/a
13DD	n/a	n/a
13DI 13DC	n/a n/a	n/a n/a
13DB	n/a	n/a
1303	n/a	n/a
1301	5.33	3.16 n/a
1004 1009	n/a n/a	n/a n/a
1003	n/a	n/a
1001A	n/a	n/a
1010	5.03	1.14
2004 1013	5.3 5.52	2.58 1.82
2005	4.86	3.56
2006	4.74	3.75
1011 001D	5.33 n/a	1.55 n/a
10DH	n/a	n/a
-	DV 151290 Slough 12	•

Manhole Reference	Manhole Cover Level	Manhole Invert Level
2011	4.53	1.22
10FA 10EJ	n/a n/a	n/a n/a
10DG	n/a	n/a
10DE	n/a	n/a
10DB	n/a	n/a
101B	n/a	n/a
10DD 20DB	n/a n/a	n/a n/a
01FD	n/a	n/a
0102A	6.44	3.38
01FG	n/a	n/a
01FH 01FI	n/a n/a	n/a n/a
01FJ	n/a	n/a
01FF	n/a	n/a
01GA	n/a	n/a
01GB 01GC	n/a n/a	n/a n/a
01BE	n/a	n/a
01BF	n/a	n/a
0003	6.02	2.89
11CB 11GI	n/a n/a	n/a n/a
11GA	n/a	n/a
11CC	n/a	n/a
11GB	n/a	n/a
11GC 11GD	n/a n/a	n/a n/a
11GD 11GE	n/a n/a	n/a n/a
11GF	n/a	n/a
11GG	n/a	n/a
10FC 11HC	n/a n/a	n/a n/a
11HA	n/a	n/a
11HD	n/a	n/a
0302	5.99	3.98
0312	n/a	2.95
0402 0301	5.17 5.75	2.45 3.69
0311	5.81	2.78
1410	5.02	1.25
141E	n/a	n/a
1411 141D	5.23 n/a	1.47 n/a
1404	5.25	1.53
141C	n/a	n/a
1312	5.55	3.33
1405 1415	5.47 n/a	2.46 n/a
1311	5.43	2.97
1403	4.55	1.3
1414	n/a	n/a
1310 1302	5.38 n/a	3.07 n/a
141H	n/a	n/a
131A	n/a	n/a
1402 141B	4.17	1.17
1418	n/a 3.58	n/a 1.08
2315	4.46	1.69
2314	3.26	1.25
2403	2.27	-5.19 2.25
2407 0212	2.81 n/a	2.25 n/a
0201B	6.49	3.67
02CI	n/a	n/a
0202	6.24	3.38
12FD 1103B	n/a 5.94	n/a 3.13
12FC	n/a	n/a
11CD	n/a	n/a
121S	6.11	5.25
12FB 12FA	n/a n/a	n/a n/a
12EJ	n/a	n/a
12EI	n/a	n/a
12EH	n/a	n/a
12EG	n/a 5.71	n/a 4.55
121L 12EF	5.71 n/a	n/a
121M	5.73	4.28
121A	5.6	3.17
12EE	n/a	n/a
The position of the apparatus shown on this plan		

The position of the apparatus shown on this plan is given without obligation and warranty, and the accuracy cannot be guaranteed. Service pipes are not shown but their presence should be anticipated. No liability of any kind whatsoever is accepted by Thames Water for any error or omission. The actual position of mains and services must be verified and established on site before any works are undertaken.



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NB. Levels quoted in metres Ordnance Newlyn Datum. The value -9999.00 indicates that no survey information is available

Manhole Reference	Manhole Cover Level	Manhole Invert Level
3701	n/a	n/a
3501A 3603	n/a 3.19	n/a 1.1
3516	n/a	n/a
3604	3.24	n/a
361A	3.5	.4
3602	3.75	.78
3601 3507	3.55 3.39	.29 n/a
3517	n/a	n/a
35CH	n/a	n/a
351A	n/a	n/a
35CG	n/a	n/a
4502 4511	n/a n/a	n/a n/a
45BF	n/a	n/a
45CB	n/a	n/a
45BH	n/a	n/a
45BG 4501	n/a n/a	n/a n/a
1705	n/a	n/a
2709	n/a	n/a
1801A	n/a	n/a
3801	n/a	n/a
1806	n/a	n/a
1814 181A	n/a n/a	n/a n/a
181B	n/a	n/a
1805	n/a	n/a
28AB	n/a	n/a
18CI 1820	n/a	n/a
1820 18CH	n/a n/a	n/a n/a
1804	n/a	n/a
28AC	n/a	n/a
28AE	n/a	n/a
28AD 1801B	n/a n/a	n/a n/a
1802	n/a	n/a
1817	n/a	n/a
1818	n/a	n/a
1816	n/a	n/a
1819	n/a	n/a
1803 1917	n/a n/a	n/a n/a
1915	n/a	n/a
191C	n/a	n/a
191B	n/a	n/a
1914	n/a	n/a
191A 1901	n/a n/a	n/a n/a
1902B	n/a	n/a
1902A	n/a	n/a
1903A	n/a	n/a
391A 1903B	n/a	n/a
491A	n/a n/a	n/a n/a
1904	n/a	n/a
391B	n/a	n/a
2538	n/a	n/a
2510 1508	n/a n/a	n/a n/a
2539	n/a	n/a
0503	n/a	n/a
151A	n/a	n/a
0502	n/a	n/a
151B 1507	n/a n/a	n/a n/a
0501	n/a n/a	n/a n/a
1510	n/a	n/a
2540	n/a	n/a
2509	n/a	n/a
1509 2536	n/a n/a	n/a n/a
2536 151D	n/a n/a	n/a n/a
	n/a	n/a
1506	n/a	n/a
151C		n/o
151C 2541	n/a	n/a
151C 2541 2534	n/a	n/a
151C 2541 2534 2508	n/a n/a	n/a n/a
151C 2541 2534	n/a	n/a
151C 2541 2534 2508 2535 2505 1505	n/a n/a n/a 2.25 n/a	n/a n/a n/a -8.8 n/a
151C 2541 2534 2508 2535 2505 1505 2507	n/a n/a n/a 2.25 n/a n/a	n/a n/a n/a -8.8 n/a n/a
151C 2541 2534 2508 2535 2505 1505 1507	n/a n/a n/a 2.25 n/a n/a 2.32	n/a n/a n/a -8.8 n/a n/a -5.24
151C 2541 2534 2508 2535 2505 1505 2507 1501 2614	n/a n/a n/a 2.25 n/a n/a 2.32 n/a	n/a n/a n/a -8.8 n/a n/a -5.24 n/a
151C 2541 2534 2508 2535 2505 1505 1507	n/a n/a n/a 2.25 n/a n/a 2.32	n/a n/a n/a -8.8 n/a n/a -5.24
151C 2541 2534 2508 2505 2505 1505 2507 1501 2614 2615	n/a n/a n/a 2.25 n/a n/a 2.32 n/a n/a	n/a n/a n/a -8.8 n/a n/a -5.24 n/a n/a

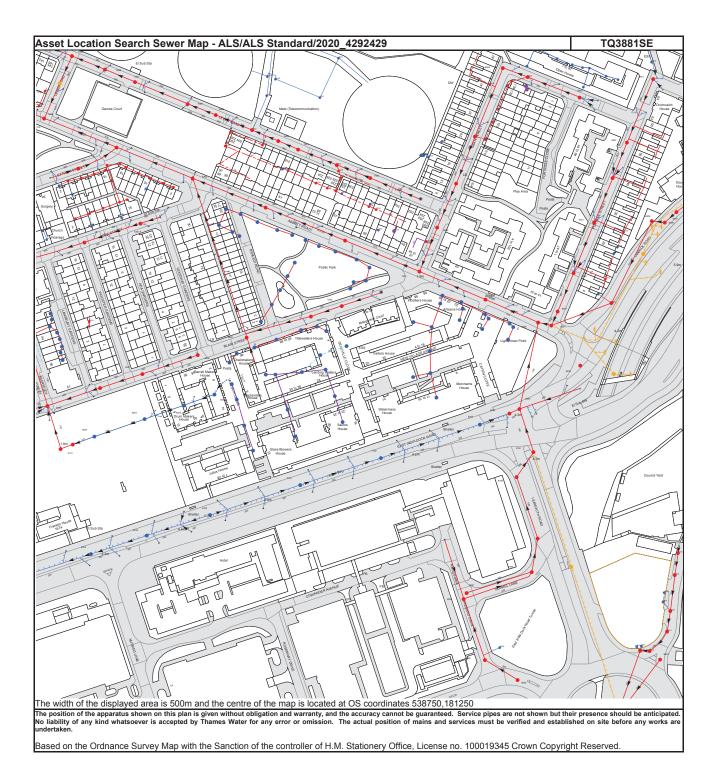
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Manhole Reference	Manhole Cover Level	Manhole Invert Level
1601	n/a	n/a
2601	n/a	n/a
2701	n/a	n/a
0702A	n/a	n/a
0701B	n/a	n/a
1708 2702	n/a n/a	n/a n/a
1707	n/a	n/a
1706	n/a	n/a
2704	n/a	n/a
2705	n/a	n/a
1702B	n/a	n/a
1701	n/a	n/a
2714	3.24	-9.46
1703	n/a	n/a
1702A	n/a	n/a
0713	n/a	n/a
2708	n/a	n/a
1704	n/a	n/a
07CH	n/a	n/a
07DB	n/a	n/a
07DD	n/a	n/a
)7DE	n/a	n/a
17DJ	n/a	n/a
)7EA	n/a	n/a
97EB	n/a	n/a
OTDI OTDI	n/a	n/a
17DH 18B I	n/a	n/a
08BJ 08CA	n/a n/a	n/a n/a
08CB	n/a n/a	n/a n/a
OSCC	n/a	n/a
D8AH	n/a	n/a
081A	n/a	n/a
08EE	n/a	n/a
)8DI	n/a	n/a
0802	n/a	n/a
)8DH	n/a	n/a
08ED	n/a	n/a
081B	n/a	n/a
08DG	n/a	n/a
08EC	n/a	n/a
081C	n/a	n/a
08DF	n/a	n/a
08EB	n/a	n/a
081D	n/a	n/a
08DE	n/a	n/a
08EA	n/a	n/a
081E	n/a	n/a
0801	n/a	n/a
091A	n/a	n/a
0901	n/a	n/a
9BD	n/a	n/a
)9BE	n/a	n/a
9BF	n/a	n/a
9CA	n/a	n/a
9BJ	n/a	n/a
9BC	n/a	n/a
)9BI	n/a	n/a
09BH	n/a	n/a
071A	n/a	n/a
0506	n/a	n/a
051C	n/a	n/a
0712 054D	n/a	n/a
051D	n/a	n/a
)7CI	n/a	n/a
0504 07AH	n/a	n/a
07AH 07BJ	n/a	n/a
07BJ 07CE	n/a n/a	n/a n/a
07CF		n/a n/a
	n/a	n/a
D7CD D7CG	n/a n/a	n/a n/a
07CC	n/a n/a	n/a n/a
07CC 051B	n/a n/a	n/a n/a
0505	n/a n/a	n/a n/a
051A	n/a n/a	n/a n/a
77.5	11/a	11/4
		•

shown but their presence should be anticipated. No liability of any kind whatsoever is accepted by Thames Water for any error or omission. The actual position of mains and services must be verified and established on site before any works are undertaken.

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NB. Levels quoted in metres Ordnance Newlyn Datum. The value -9999.00 indicates that no survey information is available

Manholo Poforonco	Manholo Cover Lovel	Manhole Invert Level
Manhole Reference 8401	Manhole Cover Level	n/a
841G	n/a	n/a
841A	n/a	n/a
841J 841B	n/a n/a	n/a n/a
8402	n/a	n/a
841C	n/a	n/a
841F	n/a	n/a
841H 841I	n/a n/a	n/a n/a
84DH	n/a	n/a
8403	n/a	n/a
94CI 94CH	n/a n/a	n/a n/a
94CJ	n/a	n/a
9404	n/a	n/a
94DA	n/a	n/a
94DC 94DB	n/a n/a	n/a n/a
9402	n/a	n/a
9401	n/a	n/a
7403	n/a	n/a
741A 741B	n/a n/a	n/a n/a
641C	n/a	n/a
641E	n/a	n/a
7402	n/a	n/a
841D 741E	n/a n/a	n/a n/a
741D	n/a	n/a
741H	n/a	n/a
741C 741G	n/a n/a	n/a n/a
741G 741F	n/a n/a	n/a n/a
7401	n/a	n/a
641D	n/a	n/a
641B 841E	n/a n/a	n/a n/a
6404	n/a	n/a
641A	n/a	n/a
6403	n/a	n/a
6402 741I	n/a n/a	n/a n/a
641F	n/a	n/a
641G	n/a	n/a
641H 741J	n/a n/a	n/a n/a
5405	n/a	n/a
9203	n/a	n/a
82CD 82CH	n/a n/a	n/a n/a
82CE	n/a	n/a
8201	n/a	n/a
82CF	n/a	n/a
8202 82CJ	n/a n/a	n/a n/a
82CI	n/a	n/a
82CG	n/a	n/a
9201	n/a	n/a
83CF 9304	n/a n/a	n/a n/a
83CE	n/a	n/a
8301	n/a	n/a
931A 931E	n/a n/a	n/a n/a
9302	n/a	n/a
931C	n/a	n/a
931B	n/a	n/a
931D 9301	n/a n/a	n/a n/a
9306	n/a	n/a
9305	n/a	n/a
9307 9403	n/a n/a	n/a n/a
72AI	n/a	n/a
731B	n/a	n/a
73CI	n/a	n/a
731C 731F	n/a n/a	n/a n/a
7303	n/a	n/a
7302	n/a	n/a
72CD 73DD	n/a	n/a n/a
73DB	n/a n/a	n/a n/a
73CG	n/a	n/a
73DA	n/a	n/a
731E 73CJ	n/a n/a	n/a n/a
731G	n/a	n/a
731D	n/a	n/a
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Manhole Reference	Manhole Cover Level	Manhole Invert Level
7311	n/a	n/a
731H	n/a	n/a
72AH	n/a	n/a
7301 831A	n/a n/a	n/a n/a
82CB	n/a	n/a
82CC	n/a	n/a
8302	n/a	n/a
83CB 83CC	n/a n/a	n/a n/a
8303	n/a	n/a
8004	n/a	n/a
8003	n/a	n/a
801A	6.29	5.79
8002 9007	n/a n/a	n/a n/a
8001	n/a	n/a
8107	n/a	n/a
8106	n/a	n/a
6102 7101	n/a n/a	n/a n/a
8105	n/a	n/a
7102	n/a	n/a
8101	n/a	n/a
61BC	n/a	n/a
62DF 62CJ	n/a n/a	n/a n/a
8205	n/a	n/a
72CB	n/a	n/a
8206	n/a	n/a
62DE	n/a	n/a
8204 62DA	n/a n/a	n/a n/a
82BJ	n/a	n/a
72CA	n/a	n/a
6203	n/a	n/a
62DB 72AG	n/a n/a	n/a n/a
62DD	n/a	n/a
62DC	n/a	n/a
82CA	n/a	n/a
72BJ 72BI	n/a n/a	n/a n/a
6202	n/a n/a	n/a n/a
63DI	n/a	n/a
63DJ	n/a	n/a
62CA	n/a	n/a
63EI 62CB	n/a n/a	n/a n/a
63FA	n/a	n/a
63EA	n/a	n/a
6201	n/a	n/a
62CE 63ED	n/a n/a	n/a n/a
62EF	n/a n/a	n/a n/a
6301	n/a	n/a
63EG	n/a	n/a
62CD	n/a	n/a
63EC 63EF	n/a n/a	n/a n/a
63EH	n/a	n/a
63EB	n/a	n/a
63EE	n/a	n/a
72BA 73CF	n/a n/a	n/a n/a
7201	n/a	n/a
731A	n/a	n/a
72AJ	n/a	n/a
73CH	n/a	n/a
72CC 53AE	n/a n/a	n/a n/a
53BG	n/a	n/a
53BH	n/a	n/a
5402	n/a	n/a
54DI 5302B	n/a n/a	n/a n/a
5302B 521A	n/a n/a	n/a n/a
53BI	n/a	n/a
54BH	n/a	n/a
53BJ	n/a	n/a
5406 54DH	n/a n/a	n/a n/a
54DJ	n/a	n/a
53CC	n/a	n/a
5401	n/a	n/a
53CA 54EA	n/a	n/a
54EA 54EB	n/a n/a	n/a n/a
53CB	n/a	n/a
5407	n/a	n/a
54EC	n/a	n/a
5301A 54ED	n/a n/a	n/a n/a
JTLD	II/Q	ıπα

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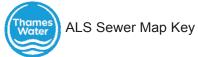
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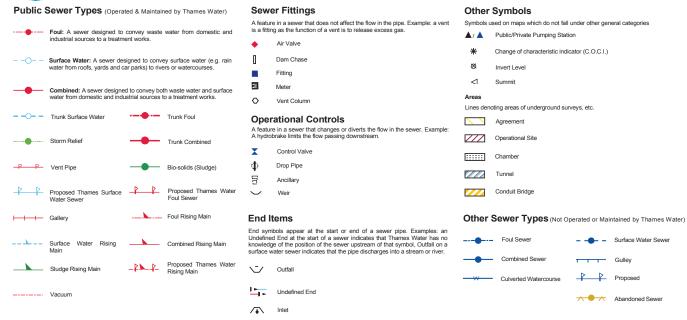
Manhole Reference	Manhole Cover Level	Manhole Invert Level
53CD	n/a	n/a
63CF	n/a	n/a
6401	n/a	n/a
6302	n/a	n/a
5101	n/a	n/a
511B	n/a	n/a
5204	n/a	n/a
5203	n/a	n/a
5205	n/a	n/a
6204	n/a	n/a
5202	n/a	n/a
5201	n/a	n/a
52CH	n/a	n/a
52CI	n/a	n/a
52CJ	n/a	n/a
52DA	n/a	n/a
52DB	n/a	n/a
5403	n/a	n/a
541A	n/a	n/a
541B	n/a	n/a
52DC	n/a	n/a
52DE	n/a	n/a
52DD	n/a	n/a
531B	n/a	n/a
531A	n/a	n/a
5103	n/a	n/a
5102	n/a	n/a
901H	5.1	4.21
901B	5.1	2.1
9011	5.1	4.39
901A	4.91	2.2
901F	5.59	4.52
901G	5.59	2.97
901C	4.96	2.37
901D	4.82	2.43
901E	4.68	2.58
911B	4.6	3.15
94DF	n/a	n/a
94DE	n/a	n/a
941A	n/a	n/a

The position of the apparatus shown on this plan is given without obligation and warranty, and the accuracy cannot be guaranteed. Service pipes are not shown but their presence should be anticipated. No liability of any kind whatsoever is accepted by Thames Water for any error or omission. The actual position of mains and services must be verified and established on site before any works are undertaken.

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6) The text appearing alongside a sewer line indicates the internal diameter of the pipe in milimetres. Text next to a manhole indicates the manhole reference number and should not be taken as a measurement. If you are unsure about any text or symbology present on the plan, please contact a member of Property Insight on 0845 070 9148.

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2) All measurements on the plans are metric.

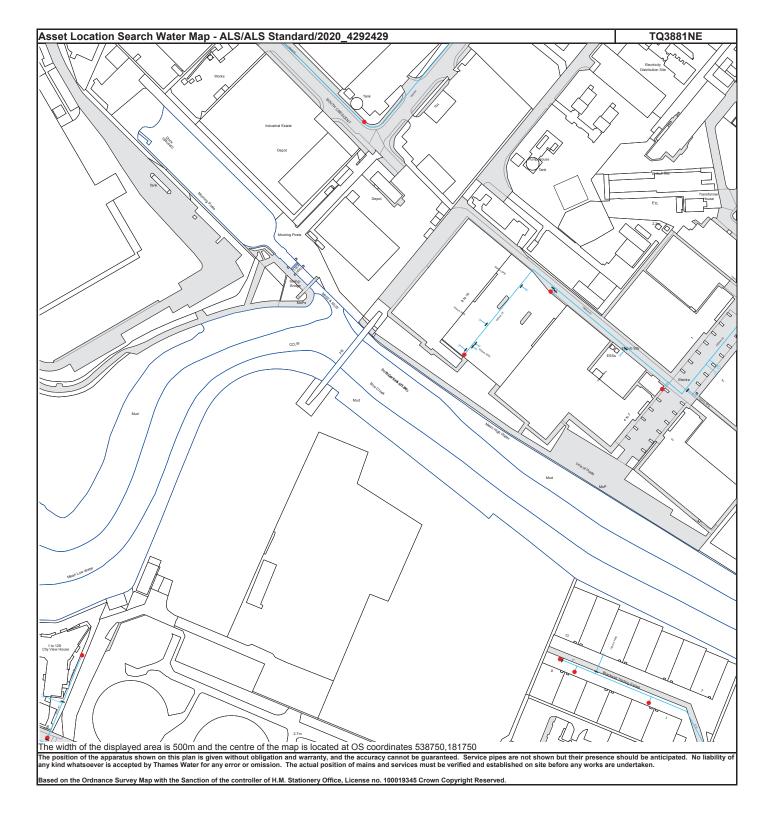
3) Arrows (on gravity fed sewers) or flecks (on rising mains) indicate direction of flow.

4) Most private pipes are not shown on our plans, as in the past, this information has not been recorded.

1) All levels associated with the plans are to Ordnance Datum Newlyn.

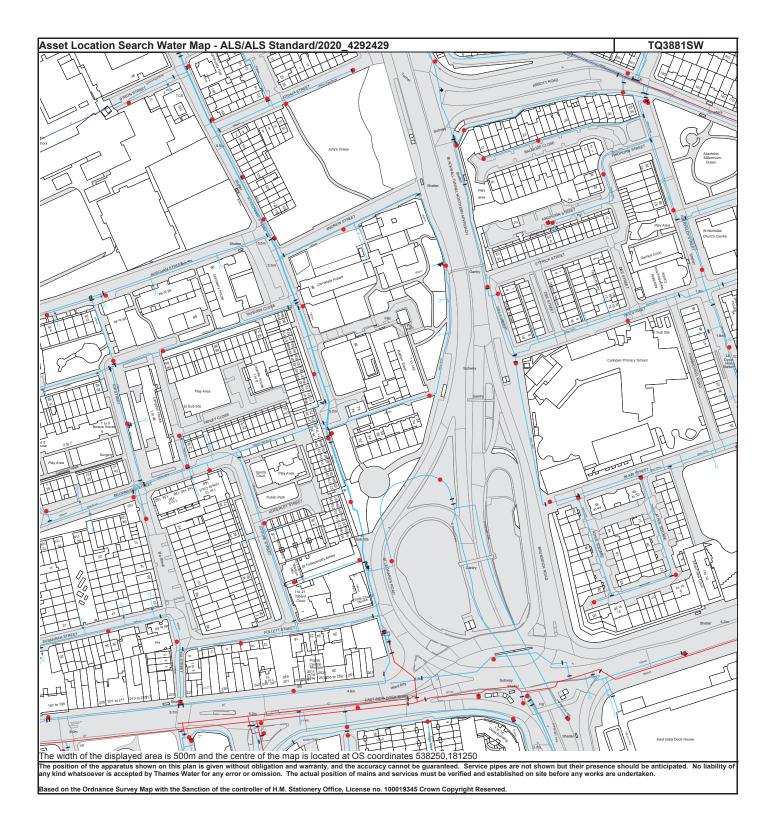
5) 'na' or '0' on a manhole level indicates that data is unavailable.

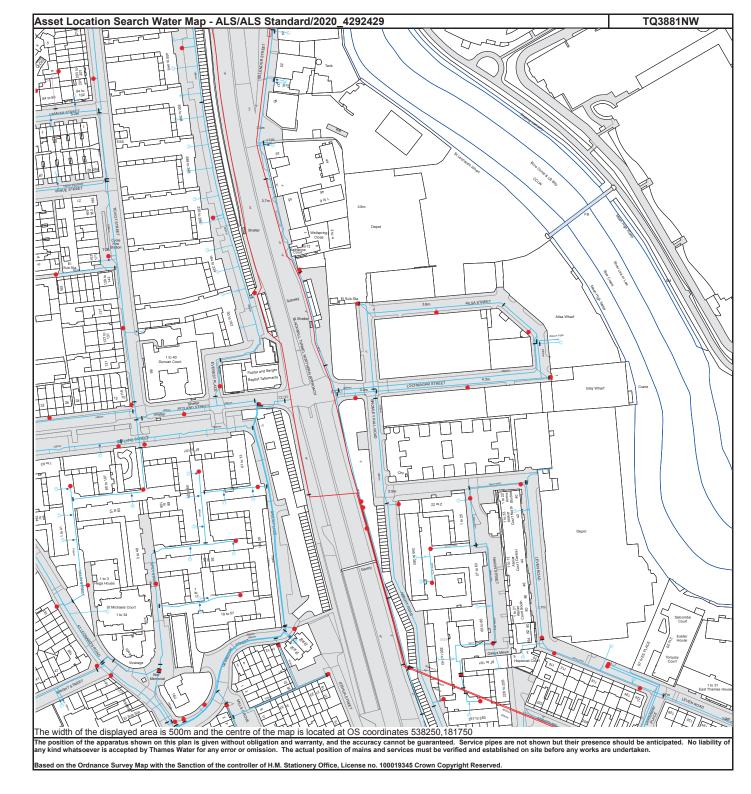
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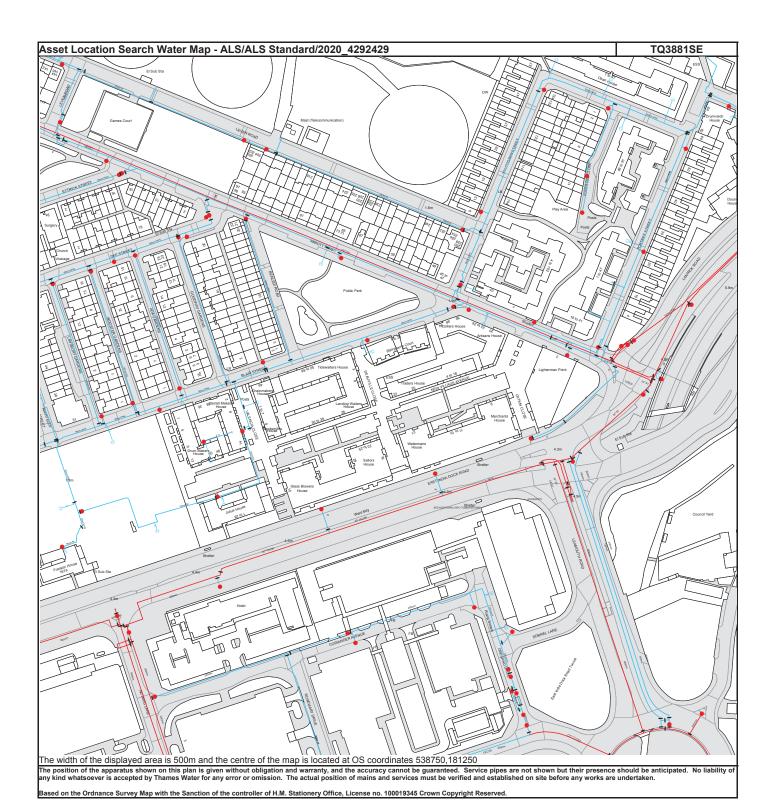


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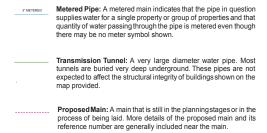
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Water Pipes (Operated & Maintained by Thames Water)

Distribution Main: The most common pipe shown on water maps. With few exceptions, domestic connections are only made to distribution mains. **Trunk Main:** A main carrying water from a source of supply to a treatment plant or reservoir, or from one treatment plant or reservoir to another. Also a main transferring water in bulk to smaller water mains used for supplying individual customers. Supply Main: A supply main indicates that the water main is used as a supply for a single property or group of properties. Fire Main: Where a pipe is used as a fire supply, the word FIRE will be displayed along the pipe.





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Valves Operational Sites General PurposeValve Booster Station → Air Valve - Other Pressure ControlValve Other (Proposed) Customer Valve ■ Pumping Station Service Reservoir Hydrants Shaft Inspection Single Hydrant Treatment Works Meters ____ Unknown Water Tower **End Items** Other Symbols Symbol indicating what happens at the end of 1 a water main. _____ Data Logger Blank Flange Capped End Emptying Pit Undefined End Manifold Customer Supply — Fire Supply Other Water Pipes (Not Operated or Maintained by Thames Water)

Other Water Company Main: Occasionally other water company water pipes may overlap the border of our clean water coverage area. These mains are denoted in purple and in most cases have the owner of the pipe displayed along them.

Private Main: Indiates that the water main in question is not owned by Thames Water. These mains normally have text associated with them indicating the diameter and owner of the pipe.

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Terms and Conditions

All sales are made in accordance with Thames Water Utilities Limited (TWUL) standard terms and conditions unless previously agreed in writing.

- 1. All goods remain in the property of Thames Water Utilities Ltd until full payment is received.
- 2. Provision of service will be in accordance with all legal requirements and published TWUL policies.
- 3. All invoices are strictly due for payment 14 days from due date of the invoice. Any other terms must be accepted/agreed in writing prior to provision of goods or service, or will be held to be invalid.
- Thames Water does not accept post-dated cheques-any cheques received will be processed for payment on date of receipt.
- 5. In case of dispute TWUL's terms and conditions shall apply.
- Penalty interest may be invoked by TWUL in the event of unjustifiable payment delay. Interest charges will be in line with UK Statute Law 'The Late Payment of Commercial Debts (Interest) Act 1998'
- 7. Interest will be charged in line with current Court Interest Charges, if legal action is taken.
- 8. A charge may be made at the discretion of the company for increased administration costs.

A copy of Thames Water's standard terms and conditions are available from the Commercial Billing Team (cashoperations@thameswater.co.uk).

We publish several Codes of Practice including a guaranteed standards scheme. You can obtain copies of these leaflets by calling us on 0800 316 9800

If you are unhappy with our service you can speak to your original goods or customer service provider. If you are not satisfied with the response, your complaint will be reviewed by the Customer Services Director. You can write to her at: Thames Water Utilities Ltd. PO Box 492, Swindon, SN38 8TU.

If the Goods or Services covered by this invoice falls under the regulation of the 1991 Water Industry Act, and you remain dissatisfied you can refer your complaint to Consumer Council for Water on 0121 345 1000 or write to them at Consumer Council for Water, 1st Floor, Victoria Square House, Victoria Square, Birmingham, B2 4AJ.

Ways to pay your bill

Credit Card	BACS Payment	Telephone Banking	Cheque
Call 0845 070 9148 quoting your invoice number starting CBA or ADS / OSS	Account number 90478703 Sort code 60-00-01 A remittance advice must be sent to: Thames Water Utilities Ltd., PO Box 3189, Slough SL1 4WW. or email ps.billing@thameswater. co.uk	By calling your bank and quoting: Account number 90478703 Sort code 60-00-01 and your invoice number	Made payable to 'Thames Water Utilities Ltd' Write your Thames Water account number on the back. Send to: Thames Water Utilities Ltd., PO Box 3189, Slough SL1 4WW or by DX to 151280 Slough 13

Thames Water Utilities Ltd Registered in England & Wales No. 2366661 Registered Office Clearwater Court, Vastern Rd, Reading, Berks, RG1 8DB.

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Mrs Maria Magdalena Burca Ecoworld and Poplar Harca C/O Meinhardt (UK) Ltd 10 Aldersgate Street London EC1A 4HJ



24 March 2021

Pre-planning enquiry: Confirmation of sufficient capacity

Dear Mrs Burca,

Thank you for providing information on your development:

Aberfeldy Village, Area known as Poplar Riverside, London, E14 0HT.

Existing: 297 dwellings, primary school and commercial space (2,217sqm).

Proposed: Demolition of existing site. Phase A – 250 residential units. Foul water discharging by gravity. 50 units to MH7303, 23 units to MH3605, 75 units to MH4301A, 102 units to MH4215. Surface water discharging by gravity attenuated to 8.59l/s to manholes 7303, 3605, 4301A and 4215.

Phase B – 573 residential units, 920.3sqm of workspace, 1,894.9sqm of residential hub, 344,8sqm of estate management space and 443.3sqm of retail space. Foul water discharging by gravity. 79 units to MH3605, 222 units to MH3517 and MH2536, 160 units to MH3516. Surface water discharging by gravity attenuated to 8l/s to manholes 3605, 3517, 2536 and 3516.

Phase C – 622 residential units and 4,816.7sqm workspace. Foul water discharging by gravity to manhole 4303. Surface water discharging by gravity attenuated to 6l/s to manhole 4303.

Phase D – Primary school. Foul water discharging by gravity to manhole 4302. Surface water discharging by gravity attenuated to 3l/s to manhole 4302.

Phase E – 427 residential units and 2,808.3sqm of workspace. Foul water discharging by gravity. 220 units to the manhole upstream of MH4203 in Blair Street, 151 units to MH4202 and 78 units to MH4216.

Overall surface water discharge rates for the development will be restricted to 33.59l/s.

We have completed the assessment of the foul water flows and surface water run-off based on the information submitted in your application with the purpose of assessing sewerage capacity within the existing Thames Water sewer network.

Thames Water Utilities Limited – Registered Office: Clearwater Court, Vastern Road, Reading RG1 8DB

Company number 02366661. VAT registration no GB 537-4569-15

Foul Water

If your proposals progress in line with the details you've provided, we're pleased to confirm that there will be sufficient sewerage capacity in the adjacent combined sewer network to serve your development.

This confirmation is valid for 12 months or for the life of any planning approval that this information is used to support, to a maximum of three years.

You'll need to keep us informed of any changes to your design – for example, an increase in the number or density of homes. Such changes could mean there is no longer sufficient capacity.

Surface Water

Please note that discharging surface water to the public sewer network should only be considered after all other methods of disposal have been investigated and proven to not be viable. In accordance with the Building Act 2000 Clause H3.3, positive connection to a public sewer will only be consented when it can be demonstrated that the hierarchy of disposal methods have been examined and proven to be impracticable. The disposal hierarchy being: 1st Soakaways; 2nd Watercourses; 3rd Sewers.

Only when it can be proven that soakage into the ground or a connection into an adjacent watercourse is not possible would we consider a restricted discharge into the public combined sewer network.

If the peak surface water run-off discharge is then restricted to Greenfield run-off rates/a maximum of 33.59l/s as your drainage strategy indicates, then we would have no objections to the proposals.

Thames Water Planning team would ask to see why it is not practicable on the site to restrict to Greenfield run-off rates if they are consulted as part of any planning application.

In considering your surface water needs, we support the use of sustainable drainage on development sites. You'll need to show the local authority and/or lead local flood authority how you've taken into account the surface water hierarchy that we've included.

Please see the attached 'Planning your wastewater' leaflet for additional information.

What happens next?

Please make sure you submit your connection application, giving us at least 21 days' notice of the date you wish to make your new connection/s.

If you've any further questions, please contact me on 0203 577 9811.

Yours sincerely

Siva Rajaratnam - Adoptions Engineer

Thames Water

Aberfeldy Village, London Masterplan, Below Ground Drainage Strategy



Appendix C – Drainage Strategy Drawings and Calculations

Proposed Surface Water Discharge rates

Total Site Area = $48334m^2 = 4.83 \text{ ha}$

Calculated Green field runoff rate = 18.8 l/s

Phase A

- 1. **Block F1:** Hard standing area (excluding green areas, roads): 2145m²
- 2. **Block H1/H2:** Hard standing area (excluding green areas, roads): 2025m²
- 3. **Block H3:** Hard standing area (excluding green areas, roads): 1700m²
- 4. **Block I1:** Hard standing area (excluding green areas, roads): 905m²
- 5. Block J1: Hard standing area (excluding green areas, roads): 2624m²

Phase B

- 1. Block A1/A2: Hard standing area (excluding green areas, roads): 3570m²
- 2. **Block A3:** Hard standing area (excluding green areas, roads): 1265m²
- 3. **Block B1/B2:** Hard standing area (excluding green areas, roads): 2225m²
- 4. **Block B3:** Hard standing area (excluding green areas, roads): 1525m²
- 5. **Block B4:** Hard standing area (excluding green areas, roads): 1255m²
- 6. **Block B5:** Hard standing area (excluding green areas, roads): 321m²

Phase C

- 1. Block C1/C2/C3/C4: Hard standing area (excluding green areas, roads): 6005m²
- 2. **Block C5:** Hard standing area (excluding green areas, roads): 210m²
- 3. **Block C6:** Hard standing area (excluding green areas, roads): 148m²
- 4. Block E1/E2/E3: Hard standing area (excluding green areas, roads): 5185m²

Phase D

1. Block D1/D2/D3/D4: Hard standing area (excluding green areas, roads): 5310m²

Phase	Storm Event	Proposed Surface Water Discharge Rate	Proposed connections For connection location refer to Proposed Discharge Location Section	Required Surface Water Attenuation
Phase A Block F1	1 in 100 year + 40% CC	1.25 l/s	1 connection	185m³
Phase A Block H1/H2	1 in 100 year + 40% CC	1.5 l/s	1 connection	161m³
Phase A Block H3	1 in 100 year + 40% CC	1.25 l/s	1 connection	135m³
Phase A Block I1	1 in 100 year + 40% CC	1 l/s	1 connection	69m³
Phase A Block J1	1 in 100 year + 40% CC	1 l/s	1 connection	260m³
Phase B Block A1/A2	1 in 100 year + 40% CC	1.5 l/s	1 connections	343m³
Phase B Block A3	1 in 100 year + 40% CC	1 l/s	Shared Connection with Block B1/B2/B4 (0.33')	98m³
Phase B Block B1/B2	1 in 100 year + 40% CC	1.5 l/s	Shared Connection with Block A3/B4 (0.33')	183m³
Phase B Block B3	1 in 100 year + 40% CC	1.3 l/s	Shared connection with Block B5 (0.5)	129m³

Phase B Block B4	1 in 100 year + 40% CC	1 l/s	Shared Connection with Block A3/B1/B2 (0.33')	97m³
Phase B Block B5	1 in 100 year + 40% CC	1 l/s	Shared connection with Block B3 (0.5)	13m³
Phase C Block C1/C2/C3/C4	1 in 100 year + 40% CC	1.5 l/s	Shared Connection with Block E1/E2/E3 & C5 (0.25)	651m³
Phase C Block C5	1 in 100 year + 40% CC	0.75 l/s	Shared Connection with Block E1/E2/E3 & C1/C2/C3/C4 (0.25)	10m³
Phase C Block C6	1 in 100 year + 40% CC	0.25 l/s	Shared Connection with Block E1/E2/E3 & C1/C2/C3/C4 (0.25)	10m³
Phase C Block E1/E2/E3	1 in 100 year + 40% CC	1.5 l/s	Shared Connection with Block C1/C2/C3/C4 & (0.25)	562m³
Phase D Block D1/D2/D3/D4	1 in 100 year + 40% CC	1.5 l/s	1 connection	576m³
Total		19.05 l/s	12 connections	3568m³

Proposed Discharge Locations

It is proposed to discharge surface water from all blocks via gravity to the surrounding Thames Water combined water sewers, the below are the locations of proposed connections and the proposed discharge rate, please also refer to the below ground drainage masterplan drawing (2812-MHT-CV-BG-DR-100);

- One new connection to the northwest corner of the building I1 into the Thames Water combined water network in Blair Street (TWMH7303); Proposed discharge rate is 1l/s;
- One new connection to the southeast corner of the building J1 into Thames Water combined water sewer in Leven Road (TWMH3602); Proposed discharge rate is 1.25l/s;
- One new connection to the northeast of building A1/A2 into the Thames Water combined water sewer in Leven Road (TWMH3605); Proposed discharge rate 1.5l/s:
- One new connection serving blocks A3, B1/B2 and B4 located to the south of the buildings discharging into Thames Water manhole (TWMH3501A); Proposed discharge rate 3.5l/s:
- One new connection north of block B3 downstream of Thames Water combined water manhole (TWMH3516); Proposed discharge rate is 2.3l/s:
- One new connection to the Thames Water combined sewer manhole in Ettrick Street (TWMH4303); Proposed discharge rate is 4l/s.
- One new connection to the Thames Water combined sewer manhole in Ettrick Street (TWMH4302); Proposed discharge rate is 1.5l/s.
- One new connection to the southeast corner of the building F1 into the Thames Water combined water sewer in Aberfeldy Street (TWMH4312); Proposed discharge rate is 1.25l/s; and
- Two new connections for Building H1&H2 and H3 which will discharge surface water via two new separate connections into Thames Water combined sewer in Aberfeldy Street (TWMH4215). Proposed discharge rate for Building H1&H2 connection is 1.5l/s and for Building H3 is 1.25l/s.

The proposed new connections are subject to a CCTV survey which will survey the line, level and condition of the existing sewers. If this survey identifies any available existing connections in those locations there may be an opportunity to reuse. This will be explored during detailed design.



www.uksuds.com | Storage estimation tool

Calculated by:	Luke Hornblow			Site Details				
Site name:	Aberfeldy Village				Latitude	:	51.5	51403° N
Site location:	Block F1				Longitud	le:		0616° W
This is an estimation of	the storage volume red	quirements that a	re needed to m	eet normal	3		0.0	JO 10 VV
best practice criteria in I for developments", SC0				•	nt Referen	ce:	4120	0047975
the non-statutory standa of drainage systems. It i volume requirements an	s recommended that h	ydraulic modellin	g software is u	sed to calcul			Jul 28 20	21 09:11
Site characteris	stics			Metho	dology			
Total site area (ha):			0.2145	esti		IH124		
Significant public ope	en space (ha):		0	Q _{BAR} est	imation method:	Calcula	ate from SPR and S	AAR
Area positively draine	ed (ha):		0.2145	SPR esti	mation method:	Calcula	ate from SOIL type	
Impermeable area (h	ıa):		0.2145	Soil ch	aracteristics			
Percentage of draine	d area that is imperr	meable (%):	100				Default	Edited
Impervious area drai	ned via infiltration (h	a):	0	SOIL typ	e:		4	4
Return period for infi	tration system desig	n (year):	10	SPR:			0.47	0.47
Impervious area drai	ned to rainwater har	vesting (ha):	0	Hydrol	ogical characte	ristics		
Return period for rain	nwater harvesting sy	stem (year):	10	Rainfall 1	00 yrs 6 hrs:		Default	Edited
Compliance factor fo	r rainwater harvestir	ng system (%):	66		00 yrs 12 hrs:			63
Net site area for store	age volume design (ha):	0.21		R conversion factor:			101.64
Net impermable area	for storage volume	design (ha):	0.21	SAAR (m			1.32	1.32
Pervious area contrib	oution to runoff (%):		30		ainfall Depth (mm):		580	580
* where rainwater harvesting that the effective impermeab				1	//и5-60/М5-2 day:		20	20
area' and the estimates of Q	_{BAR} and other flow rates will	have been reduced a	ccordingly.		cal region:		0.4	0.4
Design criteria				, ,	urve factor 1 year:		6	6
Climate change allov	vance				urve factor 10 year:		0.85	0.85
factor:	1.4				urve factor 30 year:		1.62	1.62
Urban creep allowan factor:					urve factor 100 years	.•	2.3	2.3
Volume control appro	1.1				total site area (l/s):	•	3.19	3.19
Interception rainfall d	ese leng te	rm storage)	net site area (l/s):		0.83	0.83
(mm):	5			GRAK 101	not site area (i/s).		0.83	0.83
Minimum flow rate (I/	(s): 1.25							
Site discharge r	ates	Default	Edited	Estima	ted storage vol	umes	Default	Edited
1 in 1 year (l/s):		1.3	1.3	Attenuati	on storage 1/100 yea	rs (m³):	163	163
1 in 30 years (l/s):		1.9	1.9	Long terr	n storage 1/100 years	s (m³):	22	22
1 in 100 year (l/s):		2.7	2.7	Total stor	age 1/100 years (m³)	:	185	185

This report was produced using the storage estimation tool developed by HRWallingford and available at www.uksuds.com. The use of this tool is subject to the UK SuDS terms and conditions and licence agreement, which can both be found at http://uksuds.com/terms-and-conditions.htm. The outputs from this tool have been used to estimate storage volume requirements. The use of these results is the responsibility of the users of this tool. No liability will be accepted by HR Wallingford, the Environment Agency, CEH, Hydrosolutions or any other organisation for the use of these data in the design or operational characteristics of any drainage scheme.



28/07/2021

Surface water storage requirements for sites

www.uksuds.com | Storage estimation tool

Calculated by:	Luke Hornblow	Site Details	
Site name:	Aberfeldy Village	Latitude:	51.51341° N
Site location:	Block H1/H2	Longitude:	0.00573° W
This is an estimation of	the storage volume requirements that are needed to meet normal		
•	line with Environment Agency guidance "Rainfall runoff management 030219 (2013), the SuDS Manual C753 (Ciria, 2015) and	Reference:	1349361017
	ards for SuDS (Defra, 2015). It is not to be used for detailed design is recommended that hydraulic modelling software is used to calculate	Date:	Jul 28 2021 09:09
0 ,	nd design details before finalising the design of the drainage scheme.		

Site characteristics			Methodology			
Total site area (ha):		0.2025	esti	IH124		
Significant public open space	ce (ha):	0	Q _{BAR} estimation method:	Calculate from	n SPR and S	SAAR
Area positively drained (ha)	:	0.2025	SPR estimation method:	Calculate from	n SOIL type	
Impermeable area (ha):		0.2025	Soil characteristics			
Percentage of drained area	that is impermeable (%):	100			Default	Edited
Impervious area drained via	a infiltration (ha):	0	SOIL type:		4	4
Return period for infiltration	system design (year):	10	SPR:		0.47	0.47
Impervious area drained to	rainwater harvesting (ha):	0	Hydrological characte	eristics		
Return period for rainwater	harvesting system (year):	10	Rainfall 100 yrs 6 hrs:		Default	Edited
Compliance factor for rainw	ater harvesting system (%):	66	Rainfall 100 yrs 12 hrs:			63
Net site area for storage vo	lume design (ha):	0.2	FEH / FSR conversion factor:			101.64
Net impermable area for sto	orage volume design (ha):	0.2			1.32	1.32
Pervious area contribution t	o runoff (%):	30	SAAR (mm):		580	580
· ·	ition has been used for managing surfac	e water runoff such			20	20
•	less than 50% of the 'area positively dra other flow rates will have been reduced a		'r' Ratio M5-60/M5-2 day:		0.4	0.4
Deales estad			Hydological region:		6	6
Design criteria			Growth curve factor 1 year:		0.85	0.85
Climate change allowance factor:	1.4		Growth curve factor 10 year:		1.62	1.62
Urban creep allowance			Growth curve factor 30 year:		2.3	2.3
factor:	1.1		Growth curve factor 100 years	s:	3.19	3.19
Volume control approach	Use long term storage		Q _{BAR} for total site area (I/s):		0.78	0.78
Interception rainfall depth (mm):	5		Q _{BAR} for net site area (I/s):		0.78	0.78
Minimum flow rate (l/s):	1.5					

Site discharge rates			Estimated storage volumes		
	Default	Edited	•	Default	Edited
1 in 1 year (l/s):	1.5	1.5	Attenuation storage 1/100 years (m³):	140	140
1 in 30 years (l/s):	1.8	1.8	Long term storage 1/100 years (m³):	21	21
1 in 100 year (l/s):	2.5	2.5	Total storage 1/100 years (m³):	161	161

This report was produced using the storage estimation tool developed by HRWallingford and available at www.uksuds.com. The use of this tool is subject to the UK SuDS terms and conditions and licence agreement, which can both be found at http://uksuds.com/terms-and-conditions.htm. The outputs from this tool have been used to estimate storage volume requirements. The use of these results is the responsibility of the users of this tool. No liability will be accepted by HR Wallingford, the Environment Agency, CEH, Hydrosolutions or any other organisation for the use of these data in the design or operational characteristics of any drainage scheme.



www.uksuds.com | Storage estimation tool

Calculated by:	Luke Hornblow				Site De	tails		
Site name:	Aberfeldy Village				Latitude	:	51 F	51344° N
Site location:	Block H3				Longitud			
This is an estimation of	the storage volume require	ments that ar	e needed to m	neet normal	Longitut		0.	0053° W
best practice criteria in	line with Environment Agend 330219 (2013), the SuDS Ma	cy guidance "	Rainfall runoff	management	Referen	ce:	21	0401556
the non-statutory stand	ards for SuDS (Defra, 2015) is recommended that hydra). It is not to b	e used for det	ailed design	Date:		Jul 28 20	21 09:13
	nd design details before fina	-	•					
Site characteri	stics			Methodolo	gy			
Total site area (ha):			0.17	esti		IH124		
Significant public op	en space (ha):		0	Q _{BAR} estimatio	n method:	Calculate f	rom SPR and S	AAR
Area positively drain	ed (ha):		0.17	SPR estimation	n method:	Calculate f	rom SOIL type	
Impermeable area (l	na):		0.17	Soil charac	teristics			
Percentage of draine	ed area that is impermeat	ole (%):	100		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		Default	Edited
Impervious area dra	ined via infiltration (ha):		0	SOIL type:			4	4
Return period for inf	iltration system design (ye	ear):	10	SPR:			0.47	0.47
Impervious area dra	ined to rainwater harvesti	ng (ha):	0	Hydrologic	al characte	ristics		
Return period for rai	nwater harvesting system	ı (year):	10	Rainfall 100 yrs	e 6 hre:		Default	Edited
Compliance factor for	or rainwater harvesting sy	stem (%):	66	Rainfall 100 yrs				63
Net site area for stor	rage volume design (ha):		0.17	•				101.64
Net impermable area	a for storage volume desi	gn (ha):	0.17	FEH / FSR con SAAR (mm):	iversion lactor.		1.3	1.32
Pervious area contri	bution to runoff (%):		30		Donth (name)		580	580
	g or infiltration has been used for mole area is less than 50% of the 'are						20	20
	Q _{BAR} and other flow rates will have			1 1\alio 1\io-00/	•		0.4	0.4
Design criteria				Hydological reg			6	6
Climate change allo				Growth curve for	,		0.85	0.85
factor:	1.4			Growth curve for	•		1.62	1.62
Urban creep allowar				Growth curve for	•		2.3	2.3
factor:	1.1			Growth curve fa	•	3 :	3.19	3.19
Volume control appr Interception rainfall	Osc long term s	torage		Q _{BAR} for total s	` ′		0.66	0.66
(mm):	5			Q _{BAR} for net sit	te area (i/s):		0.66	0.66
Minimum flow rate (I	/s): 1.25							
Site discharge i	rates			Estimated s	storage vol	umes		
1 in 1 year (l/s):		Default	Edited	Attenuation sto	rage 1/100 vea	rs (m³)·	Default	Edited
1 in 30 years (l/s):		1.3	1.3	Long term stora			115	118
1 in 100 years (I/s):		1.5	1.5	Total storage 1/	•	, ,	18	18
i iii 100 yeai (1/3).		2.1	2.1	Total Storage 1/	ioo years (III)	•	133	135

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Surface water storage requirements for sites

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Calculated by:	Luke Hornblow	Site Details	
Site name:	Aberfeldy Village	Latitude:	51.51300° N
Site location:	Block I1	Longitude:	0.00466° W
	f the storage volume requirements that are needed to meet normal		
	line with Environment Agency guidance "Rainfall runoff management 030219 (2013), the SuDS Manual C753 (Ciria, 2015) and	Reference:	3474697233
,	lards for SuDS (Defra, 2015). It is not to be used for detailed design is recommended that hydraulic modelling software is used to calculate	Date:	Jul 28 2021 09:18
	and design details before finalising the design of the drainage scheme.		

Site characteristics			Methodology			
Total site area (ha):		0.0905	esti	IH124		
Significant public open space	e (ha):	0	Q _{BAR} estimation method:	Calculate fron	n SPR and S	SAAR
Area positively drained (ha):		0.0905	SPR estimation method:	Calculate fron	n SOIL type	
Impermeable area (ha):		0.0905	Soil characteristics			
Percentage of drained area the	nat is impermeable (%):	100			Default	Edited
Impervious area drained via i	nfiltration (ha):	0	SOIL type:		4	4
Return period for infiltration s	ystem design (year):	10	SPR:		0.47	0.47
Impervious area drained to ra	ninwater harvesting (ha):	0	Hydrological characte	ristics		
Return period for rainwater h	arvesting system (year):	10			Default	Edited
Compliance factor for rainwa	ter harvesting system (%):	66	Rainfall 100 yrs 6 hrs:			63
Net site area for storage volu	me design (ha):	0.09	Rainfall 100 yrs 12 hrs:			101.64
Net impermable area for stor	age volume design (ha):		FEH / FSR conversion factor:		1.3	1.32
Pervious area contribution to		0.09	SAAR (mm):		580	580
* where rainwater harvesting or infiltration	` '	30 e water runoff such	M5-60 Rainfall Depth (mm):		20	20
that the effective impermeable area is le area' and the estimates of Q _{BAR} and oth	ss than 50% of the 'area positively dra	ained', the 'net site	'r' Ratio M5-60/M5-2 day:		0.4	0.4
			Hydological region:		6	6
Design criteria			Growth curve factor 1 year:		0.85	0.85
Climate change allowance	1.4		Growth curve factor 10 year:		1.62	1.62
factor: Urban creep allowance	1.4		Growth curve factor 30 year:		2.3	2.3
factor:	1.1		Growth curve factor 100 years	:	3.19	3.19
Volume control approach	Use long term storage		Q _{BAR} for total site area (l/s):		0.35	0.35
Interception rainfall depth (mm):	5		Q _{BAR} for net site area (l/s):		0.35	0.35
Minimum flow rate (I/s):	1					

Site discharge rates			Estimated storage volumes		
	Default	Edited	_	Default	Edited
1 in 1 year (l/s):	1	1	Attenuation storage 1/100 years (m³):	69	70
1 in 30 years (l/s):	1	1	Long term storage 1/100 years (m³):	0	0
1 in 100 year (l/s):	1.1	1.1	Total storage 1/100 years (m³):	69	70



www.uksuds.com | Storage estimation tool

Calculated by:	Luke	Boustead				Site Det	ails			
Site name:	Aberf	feldy Village B	Block J1			Latitude	:	51.5	51363° N	
Site location:	Towe	r Hamlets				Longitude:			0.00553° W	
This is an estimation of t	the stora	age volume requ	irements that a	re needed to m	eet normal	Ü		0.0	0333 VV	
best practice criteria in li for developments", SC03						Referen	ce:	395	1692199	
the non-statutory standa of drainage systems. It is	ards for	SuDS (Defra, 20	15). It is not to	be used for det	ailed design	Date:		Sep 17 20	21 15:08	
volume requirements an		-		-						
Site characteris	stics				Methodolo	gy				
Total site area (ha):				0.2624	esti		IH124			
Significant public ope	en spac	ce (ha):		0	Q _{BAR} estimatio	on method:	Calculate fr	om SPR and S	SAAR	
Area positively draine	ed (ha):	:		0.2624	SPR estimation	n method:	Calculate fr	om SOIL type		
Impermeable area (h	ıa):			0.2624	Soil charac	eteristics				
Percentage of draine	d area	that is imperme	eable (%):	100	oon onarac	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		Default	Edited	
Impervious area draii	ned via	infiltration (ha)):	0	SOIL type:			4	4	
Return period for infil	ltration	system design	(year):	10	SPR:			0.47	0.47	
Impervious area drain	ned to i	rainwater harve	esting (ha):	0	Hydrologic	al characte	ristics			
Return period for rain	nwater l	harvesting syst	em (year):	10	Rainfall 100 yrs	c 6 bro		Default	Edited	
Compliance factor for	r rainwa	ater harvesting	system (%):	66	Rainfall 100 yrs				63	
Net site area for stora	age vol	ume design (ha	a):	0.26	·				101.64	
Net impermable area	for sto	rage volume d	esign (ha):	0.26		nversion factor:		1.32	1.32	
Pervious area contrib	oution to	o runoff (%):		30	SAAR (mm):	Donth (name)		580	580	
* where rainwater harvesting that the effective impermeable						. , ,		20	20	
area' and the estimates of Q					'r' Ratio M5-60	-		0.4	0.4	
Design criteria					Hydological reg	-		6	6	
Climate change allow	vanaa -				Growth curve f			0.85	0.85	
factor:	varice	1.4			Growth curve f			1.62	1.62	
Urban creep allowand	ce				Growth curve f	actor 30 year:		2.3	2.3	
factor:		1				actor 100 years	: :	3.19	3.19	
Volume control appro		Flow control t	to max of 2 l/s	/ha or Qbar	Q _{BAR} for total s	site area (l/s):		1.02	1.02	
Interception rainfall d (mm):	lepth	5			Q _{BAR} for net si	te area (l/s):		1.02	1.02	
Minimum flow rate (I/	s):	1								
Site discharge r	ates				Estimated :	storage vol	umes			
			Default	Edited				Default	Edited	
1 in 1 year (l/s):			1	1	Attenuation sto	,	` /	259	259	
1 in 30 years (l/s):			1	1	Long term stora	age 1/100 years	s (m³):	0	0	
1 in 100 year (l/s).					Total storage 1	/100 years (m ³)		[050	

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Surface water storage requirements for sites

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Calculated by:	Luke Hornblow	Site Details		
Site name:	Aberfeldy Village	Latitude:	51.51676° N	
Site location:	Block A1/A2	Longitude:	0.00846° W	
	f the storage volume requirements that are needed to meet normal			
	line with Environment Agency guidance "Rainfall runoff management 030219 (2013), the SuDS Manual C753 (Ciria, 2015) and	Reference:	1572811697	
,	lards for SuDS (Defra, 2015). It is not to be used for detailed design is recommended that hydraulic modelling software is used to calculate	Date:	Jul 28 2021 09:19	
0 ,	and design details before finalising the design of the drainage scheme			

Site characteristics			Methodology				
Total site area (ha):		0.357	esti	IH124			
Significant public open spa	ce (ha):	0	Q _{BAR} estimation method:	Calculate from SPR and SAAR		SAAR	
Area positively drained (ha)):	0.357	SPR estimation method:	Calculate from	Calculate from SOIL type		
Impermeable area (ha):		0.357	Soil characteristics				
Percentage of drained area	that is impermeable (%):	100			Default	Edited	
Impervious area drained via	a infiltration (ha):	0	SOIL type:		4	4	
Return period for infiltration	system design (year):	10	SPR:		0.47	0.47	
Impervious area drained to	rainwater harvesting (ha):	0	Hydrological characte	eristics			
Return period for rainwater	harvesting system (year):	10	D-if-11 400 C b		Default	Edited	
Compliance factor for rainw	vater harvesting system (%):	66	Rainfall 100 yrs 6 hrs:			63	
Net site area for storage vo	lume design (ha):	0.36	Rainfall 100 yrs 12 hrs:			101.64	
Net impermable area for sto	orage volume design (ha):		FEH / FSR conversion factor	:	1.33	1.32	
Pervious area contribution	5	0.36	SAAR (mm):		580	580	
	ation has been used for managing surfac	30	M5-60 Rainfall Depth (mm):		20	20	
that the effective impermeable area is	s less than 50% of the 'area positively dra other flow rates will have been reduced a	ained', the 'net site	'r' Ratio M5-60/M5-2 day:		0.4	0.4	
DAK			Hydological region:		6	6	
Design criteria			Growth curve factor 1 year:		0.85	0.85	
Climate change allowance	1.4		Growth curve factor 10 year:		1.62	1.62	
factor: Urban creep allowance	1.4		Growth curve factor 30 year:		2.3	2.3	
factor:	1.1		Growth curve factor 100 year	rs:	3.19	3.19	
Volume control approach	Use long term storage		Q _{BAR} for total site area (I/s):		1.38	1.38	
Interception rainfall depth (mm):	5		Q _{BAR} for net site area (I/s):		1.38	1.38	
Minimum flow rate (l/s):	1.5						

Site discharge rates			Estimated storage volumes		
	Default	Edited	G	Default	Edited
1 in 1 year (l/s):	1.5	1.5	Attenuation storage 1/100 years (m³):	302	299
1 in 30 years (l/s):	3.2	3.2	Long term storage 1/100 years (m³):	44	44
1 in 100 year (l/s):	4.4	4.4	Total storage 1/100 years (m³):	346	343



www.uksuds.com | Storage estimation tool

Calculated by:	Luke Hornblow				Site De	tails		
Site name:	Aberfeldy Village				Latitude	: [51.5	51678° N
Site location:	Block A3				Longitude: 0.00		0758° W	
	he storage volume require							
for developments", SC03	ne with Environment Agend 30219 (2013), the SuDS Ma	anual C753 (Ciria, 2015) a	nd	Referen	ce:	128	7391727
of drainage systems. It is	rds for SuDS (Defra, 2015) s recommended that hydra d design details before fina	ulic modelling	g software is ι	ised to calculate	Date:		Jul 28 20	21 09:21
Site characteris	tics			Methodolo	ду			
Total site area (ha):			0.1265	esti		IH124		
Significant public ope	en space (ha):		0	Q _{BAR} estimatio	n method:	Calculat	te from SPR and S	AAR
Area positively draine	rea positively drained (ha):		0.1265	SPR estimation	n method:	Calculat	te from SOIL type	
Impermeable area (ha):		Ì	0.1265	Soil charac	teristics			
Percentage of draine	d area that is impermeat	ole (%):	100				Default	Edited
Impervious area drair	ned via infiltration (ha):	ĺ	0	SOIL type:			4	4
Return period for infiltration system design (year):		10	SPR:			0.47	0.47	
Impervious area drair	ned to rainwater harvesti	ng (ha):	0	Hydrological characteristics				
Return period for rainwater harvesting system (year):		10	Rainfall 100 vrs	Rainfall 100 yrs 6 hrs:		Default	Edited	
Compliance factor for	r rainwater harvesting sy	stem (%):	66	Rainfall 100 yrs 12 hrs:			63	
Net site area for stora	age volume design (ha):	ĺ	0.13	FEH / FSR conversion factor:				101.64
Net impermable area	for storage volume desi	gn (ha):	0.13	SAAR (mm):			1.33	1.32
Pervious area contrib	oution to runoff (%):	Ì	30	M5-60 Rainfall	Denth (mm):		580	580
that the effective impermeable	or infiltration has been used for me e area is less than 50% of the lare BAR and other flow rates will have	ea positively dra	ined', the 'net site	:h	. , ,		0.4	0.4
area and the estimates of ag	SAR and other new rates will have	been reduced as	ocordingly.	Hydological reg	gion:		6	6
Design criteria				Growth curve fa	actor 1 year:		0.85	0.85
Climate change allow	/ance			Growth curve fa	actor 10 year:		1.62	1.62
factor: Urban creep allowand				Growth curve fa	actor 30 year:		2.3	2.3
factor:	1.1			Growth curve fa	actor 100 years	3:	3.19	3.19
Volume control appro	each Use long term s	torage		Q _{BAR} for total s	ite area (l/s):		0.49	0.49
Interception rainfall de (mm):	epth 5			Q _{BAR} for net sit	e area (l/s):		0.49	0.49
Minimum flow rate (I/s	s): 1							
Site discharge r	ates	Default	Edited	Estimated s	storage vol	umes	Dofault	Editod
1 in 1 year (l/s):		1	1	Attenuation sto	rage 1/100 yea	ırs (m³):	Default 86	Edited 85
1 in 30 years (l/s):		1.1	1.1	Long term stora	age 1/100 years	s (m³):	13	13
1 in 100 year (l/s):		1.6	1.6	Total storage 1/	/100 years (m³)):	90	08



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Surface water storage requirements for sites

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Calculated by:	Luke Hornblow	Site Details	
Site name:	Aberfeldy Village	Latitude:	51.51599° N
Site location:	Block B1/B2	Longitude:	0.00819° W
	the storage volume requirements that are needed to meet normal		
•	line with Environment Agency guidance "Rainfall runoff management 030219 (2013), the SuDS Manual C753 (Ciria, 2015) and	Reference:	4120295627
	ards for SuDS (Defra, 2015). It is not to be used for detailed design is recommended that hydraulic modelling software is used to calculate	Date:	Jul 28 2021 09:23
volume requirements a	nd design details before finalising the design of the drainage scheme.		

	,					
Site characteristics			Methodology			
Total site area (ha):		0.2225	esti	IH124		
Significant public open space	ce (ha):	0	Q _{BAR} estimation method:	Calculate from	m SPR and S	SAAR
Area positively drained (ha)):	0.2225	SPR estimation method:	Calculate from	m SOIL type	
Impermeable area (ha):		0.2225	Soil characteristics			
Percentage of drained area	that is impermeable (%):	100			Default	Edited
Impervious area drained via	a infiltration (ha):	0	SOIL type:		4	4
Return period for infiltration	system design (year):	10	SPR:		0.47	0.47
Impervious area drained to	rainwater harvesting (ha):	0	Hydrological characte	eristics		
Return period for rainwater	harvesting system (year):	10	Rainfall 100 yrs 6 hrs:		Default	Edited
Compliance factor for rainw	vater harvesting system (%):	66	Rainfall 100 yrs 12 hrs:			63
Net site area for storage vo	lume design (ha):	0.22	FEH / FSR conversion factor:			101.64
Net impermable area for sto	orage volume design (ha):	0.22			1.33	1.32
Pervious area contribution t	to runoff (%):	30	SAAR (mm):		580	580
	ation has been used for managing surfac	e water runoff such			20	20
	less than 50% of the 'area positively dra other flow rates will have been reduced a		'r' Ratio M5-60/M5-2 day:		0.4	0.4
Danious suitania			Hydological region:		6	6
Design criteria			Growth curve factor 1 year:		0.85	0.85
Climate change allowance factor:	1.4		Growth curve factor 10 year:		1.62	1.62
Urban creep allowance			Growth curve factor 30 year:		2.3	2.3
factor:	1.1		Growth curve factor 100 year	s:	3.19	3.19
Volume control approach	Use long term storage		Q _{BAR} for total site area (I/s):		0.86	0.86
Interception rainfall depth (mm):	5		Q _{BAR} for net site area (I/s):		0.86	0.86
Minimum flow rate (l/s):	1.5					

Site discharge rates			Estimated storage volumes		
_	Default	Edited	•	Default	Edited
1 in 1 year (l/s):	1.5	1.5	Attenuation storage 1/100 years (m³):	161	160
1 in 30 years (l/s):	2	2	Long term storage 1/100 years (m³):	23	23
1 in 100 year (l/s):	2.7	2.7	Total storage 1/100 years (m³):	185	183



www.uksuds.com | Storage estimation tool

Luke Hornblow			Site Details					
Site name:	Aberfeldy Village				Latitude	:	51.5	51486° N
Site location:	Block B3				Longitud	de:		0776° W
This is an estimation of th best practice criteria in lin for developments", SC030 the non-statutory standard of drainage systems. It is volume requirements and	e with Environment Agen 0219 (2013), the SuDS M ds for SuDS (Defra, 2015 recommended that hydra	cy guidance " anual C753 (). It is not to b ulic modelling	'Rainfall runoff Ciria, 2015) ar se used for det g software is u	management id ailed design sed to calculate	Referen Date:	ce:		8750634
Site characterist	ics			Methodolog	ду			
Total site area (ha):			0.1525	esti		IH124		
Significant public oper	n space (ha):		0	Q _{BAR} estimation	n method:		e from SPR and S	SAAR
Area positively drained (ha):			0.1525	SPR estimation	n method:		from SOIL type	
Impermeable area (ha):			0.1525	Soil charac	torictics		- 71	
Percentage of drained	area that is impermeal	ble (%):	100	Son Charac	leristics		Default	Edited
Impervious area drain	ed via infiltration (ha):		0	SOIL type:			4	4
Return period for infiltr	ration system design (y	ear):	10	SPR:			0.47	0.47
Impervious area drain	ed to rainwater harvest	ing (ha):	0	Hydrologic	al characte	ristics		
Return period for rainv	vater harvesting system	n (year):	10	Painfall 100 yrs	6 bro		Default	Edited
Compliance factor for	rainwater harvesting sy	vstem (%):	66	Rainfall 100 yrs				63
Net site area for storaç	ge volume design (ha):		0.15	Rainfall 100 yrs 12 hrs: FEH / FSR conversion factor:			101.64	
Net impermable area f	for storage volume desi	ign (ha):	0.15		version factor:		1.32	1.32
Pervious area contribu	ution to runoff (%):		30	SAAR (mm):	Danth (nama)		580	580
	r infiltration has been used for n area is less than 50% of the 'ar				. , ,		20	20
	R and other flow rates will have			'r' Ratio M5-60/	•		0.4	0.4
Design criteria				Hydological reg			6	6
•				Growth curve fa	,		0.85	0.85
Climate change allowated factor:	1.4			Growth curve fa	•		1.62	1.62
Urban creep allowance	е			Growth curve fa	•		2.3	2.3
factor:	1.1			Growth curve fa	•	3:	3.19	3.19
Volume control approa	ess ising terms	torage		Q _{BAR} for total s	, ,		0.59	0.59
Interception rainfall de (mm):	pth 5			Q _{BAR} for net sit	e area (l/s):		0.59	0.59
Minimum flow rate (I/s): 1.3							
Site discharge ra	tes			Estimated s	storage vol	umes		
1 in 1 year (l/s):		Default	Edited	Attenuation sto	rage 1/100 voo	ure (m³\.	Default	Edited
1 in 30 years (l/s):		1.3	1.3	Long term stora			113	113
1 in 100 years (l/s):		1.4	1.4	Total storage 1/	,	,	16	16
i iii 100 year (i/s).		1.9	1.9	Total Storage 1/	100 years (m°).	129	129

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28/07/2021

Surface water storage requirements for sites

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Calculated by:	Luke Hornblow	Site Details	
Site name:	Aberfeldy Village	Latitude:	51.51562° N
Site location:	Block B4	Longitude:	0.00723° W
	f the storage volume requirements that are needed to meet normal		
	line with Environment Agency guidance "Rainfall runoff management 030219 (2013), the SuDS Manual C753 (Ciria, 2015) and	Reference:	2940151236
,	lards for SuDS (Defra, 2015). It is not to be used for detailed design is recommended that hydraulic modelling software is used to calculate	Date:	Jul 28 2021 09:26
0 ,	and design details before finalising the design of the drainage scheme.		

Site characteristics			Methodology			
Total site area (ha):		0.1255	esti	IH124		
Significant public open spac	ce (ha):	0	Q _{BAR} estimation method:	Calculate from	SAAR	
Area positively drained (ha)	:	0.1255	SPR estimation method:	Calculate from		
Impermeable area (ha):		0.1255	Soil characteristics			
Percentage of drained area	that is impermeable (%):	100			Default	Edited
Impervious area drained via	a infiltration (ha):	0	SOIL type:		4	4
Return period for infiltration	system design (year):	10	SPR:		0.47	0.47
Impervious area drained to	rainwater harvesting (ha):	0	Hydrological characte	eristics		
Return period for rainwater	harvesting system (year):	10	Rainfall 100 yrs 6 hrs:		Default	Edited
Compliance factor for rainw	rater harvesting system (%):	66	,			63
Net site area for storage vo	lume design (ha):	0.13	Rainfall 100 yrs 12 hrs:			101.64
Net impermable area for sto	orage volume design (ha):	0.13	FEH / FSR conversion factor:		1.33	1.32
Pervious area contribution t	to runoff (%):	30	SAAR (mm):		580	580
	ation has been used for managing surfac	e water runoff such	M5-60 Rainfall Depth (mm):		20	20
•	less than 50% of the 'area positively dra other flow rates will have been reduced a		'r' Ratio M5-60/M5-2 day:		0.4	0.4
			Hydological region:		6	6
Design criteria			Growth curve factor 1 year:		0.85	0.85
Climate change allowance factor:	1.4		Growth curve factor 10 year:		1.62	1.62
Urban creep allowance			Growth curve factor 30 year:		2.3	2.3
factor:	1.1		Growth curve factor 100 year	rs:	3.19	3.19
Volume control approach	Use long term storage		Q _{BAR} for total site area (I/s):		0.49	0.49
Interception rainfall depth (mm):	5		Q _{BAR} for net site area (l/s):		0.49	0.49
Minimum flow rate (I/s):	1					

Site discharge rates		Estimated storage volumes			
	Default	Edited	•	Default	Edited
1 in 1 year (l/s):	1	1	Attenuation storage 1/100 years (m³):	85	84
1 in 30 years (l/s):	1.1	1.1	Long term storage 1/100 years (m³):	13	13
1 in 100 year (l/s):	1.6	1.6	Total storage 1/100 years (m³):	98	97



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Calculated by:	Luke Hornblow			Site Details				
Site name:	Aberfeldy Village				Latitude:		51.51494° N	
Site location:	Block B5				Longitud	le:		0801° W
	f the storage volume requirer							
for developments", SC	line with Environment Agend 030219 (2013), the SuDS Ma	anual C753 (Ciria, 2015) an	nd	Referen	ce:	304	0714113
of drainage systems. It	dards for SuDS (Defra, 2015) t is recommended that hydrat and design details before fina	ulic modelling	g software is u	sed to calculate	Date:		Aug 18 20	21 12:02
Site character	istics			Methodolo	gy			
Total site area (ha):			0.0321	esti		IH124		
Significant public or	oen space (ha):		0	Q _{BAR} estimation	n method:	Calculate	e from SPR and S	AAR
Area positively drain	ned (ha):	Ì	0.0321	SPR estimation	n method:	Calculate	e from SOIL type	
Impermeable area ((ha):		0.0321	Soil charac	cteristics			
Percentage of drain	ed area that is impermeat	ole (%):	100				Default	Edited
Impervious area dra	ained via infiltration (ha):		0	SOIL type:			4	4
Return period for in	filtration system design (ye	ear):	10	SPR:			0.47	0.47
Impervious area dra	ained to rainwater harvesti	ng (ha):	0	Hydrologic	al characte	ristics		
Return period for ra	inwater harvesting system	ı (year):	10	Rainfall 100 yrs	s 6 hrs:		Default	Edited
Compliance factor f	or rainwater harvesting sy	stem (%):	66	Rainfall 100 yrs				63
Net site area for sto	orage volume design (ha):		0.03	FEH / FSR cor			4.00	83.16
Net impermable are	ea for storage volume desi	gn (ha):	0.03	SAAR (mm):			1.32	1.08
Pervious area contr	ibution to runoff (%):		30	M5-60 Rainfall	Depth (mm):		580	580
that the effective impermea	ng or infiltration has been used for m able area is less than 50% of the 'are Q _{BAR} and other flow rates will have l	ea positively dra	ined', the 'net site	'r' Ratio M5-60	, , ,		0.4	0.4
	GBAR GITG GETS. HOW TOLOG TILL HAVE	200111044004	ooorag.y.	Hydological reg	gion:		6	6
Design criteria	1			Growth curve f	actor 1 year:		0.85	0.85
Climate change allo	owance 1.4			Growth curve f	actor 10 year:		1.62	1.62
Urban creep allowa				Growth curve f	actor 30 year:		2.3	2.3
factor:	1.1			Growth curve f	actor 100 years	:	3.19	3.19
Volume control app	roach Use long term st	torage		Q _{BAR} for total s	site area (l/s):		0.12	0.12
Interception rainfall (mm):	depth 5			Q _{BAR} for net si	te area (l/s):		0.12	0.12
Minimum flow rate ((l/s): 1							
Site discharge	rates	Default	Edited	Estimated	storage vol	umes	Default	Edited
1 in 1 year (l/s):		1	1	Attenuation sto	orage 1/100 yea	rs (m³):	16	13
1 in 30 years (l/s):		1	1	Long term stora	age 1/100 years	s (m³):	0	0
1 in 100 year (I/s):		1	1	Total storage 1	/100 years (m³)	:	16	13

This report was produced using the storage estimation tool developed by HRWallingford and available at www.uksuds.com. The use of this tool is subject to the UK SuDS terms and conditions and licence agreement, which can both be found at http://uksuds.com/terms-and-conditions.htm. The outputs from this tool have been used to estimate storage volume requirements. The use of these results is the responsibility of the users of this tool. No liability will be accepted by HR Wallingford, the Environment Agency, CEH, Hydrosolutions or any other organisation for the use of these data in the design or operational characteristics of any drainage scheme.



28/07/2021

Surface water storage requirements for sites

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Calculated by:	Luke Hornblow	Site Details	
Site name:	Aberfeldy Village	Latitude:	51.51448° N
Site location:	Block C1/C2/C3/C4	Longitude:	0.00776° W
	f the storage volume requirements that are needed to meet normal		
	line with Environment Agency guidance "Rainfall runoff management 030219 (2013), the SuDS Manual C753 (Ciria, 2015) and	Reference:	632757355
	lards for SuDS (Defra, 2015). It is not to be used for detailed design is recommended that hydraulic modelling software is used to calculate	Date:	Jul 28 2021 09:30
0 ,	and design details before finalising the design of the drainage scheme.		

Site characteristics	Site characteristics			Methodology			
Total site area (ha):		0.6005	esti	IH124			
Significant public open spa	ce (ha):	0	Q _{BAR} estimation method:	Calculate fron	n SPR and S	SAAR	
Area positively drained (ha)):	0.6005	SPR estimation method:	Calculate from SOIL type			
Impermeable area (ha):		0.6005	Soil characteristics				
Percentage of drained area	that is impermeable (%):	100			Default	Edited	
Impervious area drained via	a infiltration (ha):	0	SOIL type:		4	4	
Return period for infiltration	system design (year):	10	SPR:		0.47	0.47	
Impervious area drained to	rainwater harvesting (ha):	0	Hydrological characte	ristics			
Return period for rainwater	harvesting system (year):	10			Default	Edited	
Compliance factor for rainw	vater harvesting system (%):	66	Rainfall 100 yrs 6 hrs:			63	
Net site area for storage vo	lume design (ha):	0.6	Rainfall 100 yrs 12 hrs:			101.64	
Net impermable area for sto	orage volume design (ha):		FEH / FSR conversion factor: SAAR (mm):		1.32	1.32	
Pervious area contribution		0.6			580	580	
	ation has been used for managing surfac	30 se water runoff such	M5-60 Rainfall Depth (mm):		20	20	
that the effective impermeable area is	less than 50% of the 'area positively dra other flow rates will have been reduced a	ained', the 'net site	'r' Ratio M5-60/M5-2 day:		0.4	0.4	
		0,7	Hydological region:		6	6	
Design criteria			Growth curve factor 1 year:		0.85	0.85	
Climate change allowance	1.4		Growth curve factor 10 year:		1.62	1.62	
factor: Urban creep allowance	1.4		Growth curve factor 30 year:		2.3	2.3	
factor:	1.1		Growth curve factor 100 years	:	3.19	3.19	
Volume control approach	Use long term storage		Q _{BAR} for total site area (l/s):		2.33	2.33	
Interception rainfall depth (mm):	5		Q _{BAR} for net site area (l/s):		2.33	2.33	
Minimum flow rate (I/s):	1.5						

Site discharge rates			Estimated storage volumes		
	Default	Edited	•	Default	Edited
1 in 1 year (l/s):	2	2	Attenuation storage 1/100 years (m³):	526	526
1 in 30 years (l/s):	5.4	5.4	Long term storage 1/100 years (m³):	125	125
1 in 100 year (l/s):	7.4	7.4	Total storage 1/100 years (m³):	651	651



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Calculated by:	Luke Hornblow			Site Det	ails			
Site name:	Aberfeldy Village				Latitude	: [51 <i>5</i>	51494° N
Site location:	Block C5				Longitud	de:		0801° W
best practice criteria in li for developments", SC03 the non-statutory standa of drainage systems. It is	he storage volume require ne with Environment Ager 30219 (2013), the SuDS N rds for SuDS (Defra, 2015 is recommended that hydra d design details before fin	ncy guidance ' lanual C753 (6). It is not to b aulic modelling	'Rainfall runot Ciria, 2015) a be used for de g software is ι	ff management nd stailed design used to calculat	Referen Date:			7012526
Site characteris		anonig are de	g oo a	Method				
Total site area (ha):		(0.0210	esti		IH124		
Significant public ope	n space (ha):		0	Q _{BAR} estim	nation method:		e from SPR and S	SAAR
Area positively drained (ha):			0.021		ation method:		e from SOIL type	7011
Impermeable area (ha):			0.021	Soil cha	racteristics			
Percentage of draine	d area that is impermea	ble (%):	100	Soli Cila	racteristics		Default	Edited
Impervious area drained via infiltration (ha):			0	SOIL type:	SOIL type:			4
Return period for infiltration system design (year):		10	SPR:			0.47	0.47	
Impervious area drained to rainwater harvesting (ha): Return period for rainwater harvesting system (year):			0	Hydrolo	gical characte	ristics		
			10	Painfall 10	Rainfall 100 yrs 6 hrs:		Default	Edited
Compliance factor for	rainwater harvesting s	ystem (%):	66		00 yrs 12 hrs: R conversion factor:			63
Net site area for stora	age volume design (ha):		0.02					83.16
Net impermable area	for storage volume des	ign (ha):	0.02	SAAR (mm): M5-60 Rainfall Depth (mm):		1.32	1.08	
Pervious area contrib	oution to runoff (%):	ĺ	30				580	580
that the effective impermeable	or infiltration has been used for a e area is less than 50% of the 'a _{SAR} and other flow rates will have	rea positively dra	ined', the 'net site	ch -	5-60/M5-2 day:		0.4	0.4
area and the commutes of ap	sak and stills her rates ill have	. 20011 1000000	ooorag.y.	Hydologica	al region:		6	6
Design criteria				Growth cur	ve factor 1 year:		0.85	0.85
Climate change allow	vance			Growth cur	ve factor 10 year:		1.62	1.62
factor: Urban creep allowand				Growth cur	ve factor 30 year:		2.3	2.3
factor:	1.1			Growth cur	ve factor 100 years	s:	3.19	3.19
Volume control appro	use long term s	storage		Q _{BAR} for to	tal site area (l/s):		0.08	0.08
Interception rainfall d (mm):	epth 5			Q _{BAR} for no	et site area (l/s):		0.08	0.08
Minimum flow rate (I/	s): 0.75							
Site discharge r	ates	Default	E dita d	Estimate	ed storage vol	umes	Default	
1 in 1 year (l/s):		Default 0.8	Edited 0.8	Attenuation	n storage 1/100 yea	rs (m³):	Default 10	Edited 8
1 in 30 years (l/s):		0.8	0.8	₹	storage 1/100 years		0	0
1 in 100 vear (l/s):		0.0	0.0	Total storag	ge 1/100 vears (m³)	:	10	

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18/08/2021

HR Wallingford

Surface water storage requirements for sites

www.uksuds.com | Storage estimation tool

Calculated by:	Luke Hornblow	Site Details	
Site name:	Aberfeldy Village	Latitude:	51.51434° N
Site location:	Block C6	Longitude:	0.00799° W
	f the storage volume requirements that are needed to meet normal		
	line with Environment Agency guidance "Rainfall runoff management 030219 (2013), the SuDS Manual C753 (Ciria, 2015) and	Reference:	4129630892
•	lards for SuDS (Defra, 2015). It is not to be used for detailed design is recommended that hydraulic modelling software is used to calculate	Date:	Aug 18 2021 10:42
	and design details before finalising the design of the drainage scheme.		

Site characteristics			Methodology			
Total site area (ha):		0.0148	esti	IH124		
Significant public open spa	ce (ha):	0	Q _{BAR} estimation method:	Calculate from	n SPR and S	SAAR
Area positively drained (ha)):	0.0148	SPR estimation method:	Calculate fror	n SOIL type	
Impermeable area (ha):		0.0148	Soil characteristics			
Percentage of drained area	that is impermeable (%):	100	Con characteristics		Default	Edited
Impervious area drained via	a infiltration (ha):	0	SOIL type:		4	4
Return period for infiltration	system design (year):	10	SPR:		0.47	0.47
Impervious area drained to	rainwater harvesting (ha):	0	Hydrological characte	ristics		
Return period for rainwater	harvesting system (year):	10	D-i-f-II 400 C b		Default	Edited
Compliance factor for rainw	vater harvesting system (%):	66	Rainfall 100 yrs 6 hrs:			63
Net site area for storage vo	lume design (ha):	0.02	Rainfall 100 yrs 12 hrs: FEH / FSR conversion factor:			101.64
Net impermable area for sto	orage volume design (ha):	0.01			1.32	1.32
Pervious area contribution	to runoff (%):	30	SAAR (mm):		580	580
	ation has been used for managing surfac	ce water runoff such	M5-60 Rainfall Depth (mm):		20	20
-	less than 50% of the 'area positively dra other flow rates will have been reduced a		'r' Ratio M5-60/M5-2 day:		0.4	0.4
			Hydological region:		6	6
Design criteria			Growth curve factor 1 year:		0.85	0.85
Climate change allowance factor:	1.4		Growth curve factor 10 year:		1.62	1.62
Urban creep allowance			Growth curve factor 30 year:		2.3	2.3
factor:	1.1		Growth curve factor 100 years	s:	3.19	3.19
Volume control approach	Use long term storage		Q _{BAR} for total site area (I/s):		0.06	0.06
Interception rainfall depth (mm):	5		Q _{BAR} for net site area (I/s):		0.08	0.08
Minimum flow rate (I/s):	0.25					
						

Site discharge rates			Estimated storage volumes		
	Default	Edited	•	Default	Edited
1 in 1 year (l/s):	0.3	0.3	Attenuation storage 1/100 years (m³):	10	10
1 in 30 years (l/s):	0.3	0.3	Long term storage 1/100 years (m³):	0	0
1 in 100 year (l/s):	0.3	0.3	Total storage 1/100 years (m³):	10	10



www.uksuds.com | Storage estimation tool

Calculated by: Luke Hornblow					Site Details					
Site name:	Aberfe	ldy Villag	ge				Latitude		51.51448° N	
Site location:	Block I	Block E1/E2/E3					Langituda		0776° W	
This is an estimation of	the storag	je volume i	requireme	ents that ar	e needed to m	eet normal	· ·		0.0	0770 VV
best practice criteria in I for developments", SC0				•		•	Referen	ce:	29	4567894
the non-statutory standa of drainage systems. It volume requirements ar	is recomm	ended tha	ıt hydrauli	c modelling	software is u	sed to calculate	Date:		Jul 28 20	21 09:34
Site characteris	stics					Methodolo	ogy			
Total site area (ha):					0.5185	esti		IH124		
Significant public ope	en space	(ha):			0	Q _{BAR} estimation	on method:		om SPR and S	SAAR
Area positively drain	ed (ha):				0.5185	SPR estimation	on method:	Calculate fr	om SOIL type	
Impermeable area (h	na):				0.5185	Soil chara	ctaristics			
Percentage of draine	ed area th	nat is impe	ermeable	e (%):	100	Oon chara	Cicristics		Default	Edited
Impervious area drai	ined via i	nfiltration	(ha):		0	SOIL type:			4	4
Return period for infi	iltration s	ystem des	sign (yea	ır):	10	SPR:			0.47	0.47
Impervious area drained to rainwater harvesting (ha):		0	Hydrological characteristics							
Return period for rainwater harvesting system (year):		year):	10	Rainfall 100 yrs 6 hrs: Rainfall 100 yrs 12 hrs:		Default	Edited			
Compliance factor for rainwater harvesting system (%):		em (%):	66				63			
Net site area for stor	age volu	me desigr	n (ha):		0.52	FEH / FSR conversion factor:				101.64
Net impermable area	a for stora	age volum	ne desigr	n (ha):	0.52		nversion factor:		1.32	1.32
Pervious area contril	bution to	runoff (%)):		30	SAAR (mm):	II D . II . ()		580	580
* where rainwater harvesting that the effective impermeat					water runoff sucl	า	ll Depth (mm):		20	20
area' and the estimates of Q						'r' Ratio M5-60	•		0.4	0.4
Design criteria						Hydological re			6	6
•						Growth curve	•		0.85	0.85
Climate change allow factor:	wance	1.4				Growth curve	factor 10 year:		1.62	1.62
Urban creep allowan	nce					Growth curve	factor 30 year:		2.3	2.3
factor:		1.1]			Growth curve	factor 100 years	:	3.19	3.19
Volume control appro		Use long	term sto	rage		Q _{BAR} for total	site area (l/s):		2.01	2.01
Interception rainfall of (mm):		5				Q _{BAR} for net s	ite area (l/s):		2.01	2.01
Minimum flow rate (I	/s):	1.5								
Site discharge r	rates					Estimated	storage vol	ımes		
2.10 2.1001141901				Default	Edited		_		Default	Edited
1 in 1 year (l/s):				1.7	1.7	Attenuation st	orage 1/100 yea	rs (m³):	454	454
1 in 30 years (l/s):				4.6	4.6	Long term sto	rage 1/100 years	s (m³):	108	108
The same of the sa					W .	1				

Site discharge rates			Estimated storage volumes		
	Default	Edited	· ·	Default	Edited
1 in 1 year (l/s):	1.7	1.7	Attenuation storage 1/100 years (m³):	454	454
1 in 30 years (l/s):	4.6	4.6	Long term storage 1/100 years (m³):	108	108
1 in 100 year (l/s):	6.4	6.4	Total storage 1/100 years (m³):	562	562

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28/07/2021

Surface water storage requirements for sites

www.uksuds.com | Storage estimation tool

Calculated by:	Luke Hornblow	Site Details	
Site name:	Aberfeldy Village	Latitude:	51.51448° N
Site location:	Block D1/D2/D3/D4	Longitude:	0.00776° W
This is an estimation of	f the storage volume requirements that are needed to meet normal		
	line with Environment Agency guidance "Rainfall runoff management 030219 (2013), the SuDS Manual C753 (Ciria, 2015) and	Reference:	1709419245
,	lards for SuDS (Defra, 2015). It is not to be used for detailed design is recommended that hydraulic modelling software is used to calculate	Date:	Jul 28 2021 09:36
0 ,	and design details before finalising the design of the drainage scheme.		

Site characteristics	Site characteristics			Methodology			
Total site area (ha):		0.531	esti	IH124			
Significant public open space (ha):		0	Q _{BAR} estimation method: Calculate		from SPR and SAAR		
Area positively drained (ha):	0.531	SPR estimation method:	Calculate from	n SOIL type		
Impermeable area (ha):		0.531	Soil characteristics				
Percentage of drained area	that is impermeable (%):	100	oon onaraotoriotioo		Default	Edited	
Impervious area drained via	a infiltration (ha):	0	SOIL type:		4	4	
Return period for infiltration	system design (year):	10	SPR:		0.47	0.47	
Impervious area drained to	rainwater harvesting (ha):	0	Hydrological characte	eristics			
Return period for rainwater	harvesting system (year):	10	D-ifII 400 C h		Default	Edited	
Compliance factor for rainw	vater harvesting system (%):	66	Rainfall 100 yrs 6 hrs:			63	
Net site area for storage vo	lume design (ha):	0.53	Rainfall 100 yrs 12 hrs:			101.64	
Net impermable area for st	orage volume design (ha):	0.53	FEH / FSR conversion factor		1.32	1.32	
Pervious area contribution	to runoff (%):	30	SAAR (mm):		580	580	
	ation has been used for managing surfac	e water runoff such	M5-60 Rainfall Depth (mm):		20	20	
•	s less than 50% of the 'area positively dra other flow rates will have been reduced a		'r' Ratio M5-60/M5-2 day:		0.4	0.4	
			Hydological region:		6	6	
Design criteria			Growth curve factor 1 year:		0.85	0.85	
Climate change allowance factor:	1.4		Growth curve factor 10 year:		1.62	1.62	
Urban creep allowance			Growth curve factor 30 year:		2.3	2.3	
factor:	1.1		Growth curve factor 100 year	rs:	3.19	3.19	
Volume control approach	Use long term storage		Q _{BAR} for total site area (I/s):		2.06	2.06	
Interception rainfall depth (mm):	5		Q _{BAR} for net site area (I/s):		2.06	2.06	
Minimum flow rate (l/s):	1 5						

Site discharge rates			Estimated storage volumes		
	Default	Edited	_	Default	Edited
1 in 1 year (l/s):	1.7	1.7	Attenuation storage 1/100 years (m³):	465	465
1 in 30 years (l/s):	4.7	4.7	Long term storage 1/100 years (m³):	110	110
1 in 100 year (l/s):	6.6	6.6	Total storage 1/100 years (m³):	576	576